

# FEM solution for example problem of stationary heat flow

Piotr Pluciński

e-mail: [Piotr.Plucinski@pk.edu.pl](mailto:Piotr.Plucinski@pk.edu.pl)

Jerzy Pamin

e-mail: [Jerzy.Pamin@pk.edu.pl](mailto:Jerzy.Pamin@pk.edu.pl)

Chair for Computational Engineering

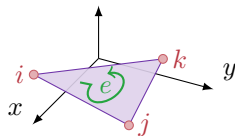
Faculty of Civil Engineering, Cracow University of Technology

URL: [www.CCE.pk.edu.pl](http://www.CCE.pk.edu.pl)

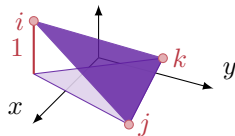
# Determination of shape functions for 3-node element

Shape function  $N_i(x, y) = \alpha_{1i} + \alpha_{2i}x^e + \alpha_{3i}y^e$

$$\begin{bmatrix} 1 & x_i & y_i \\ 1 & x_j & y_j \\ 1 & x_k & y_k \end{bmatrix} \begin{bmatrix} \alpha_{1i} \\ \alpha_{2i} \\ \alpha_{3i} \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$



$N_i(x^e, y^e)$

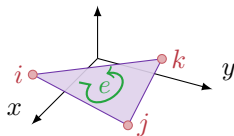


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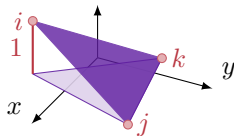
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$$W = \begin{vmatrix} 1 & x_i & y_i \\ 1 & x_j & y_j \\ 1 & x_k & y_k \end{vmatrix} = 2P_{\Delta}$$



$N_i(x^e, y^e)$



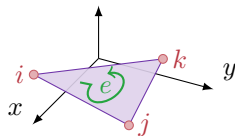
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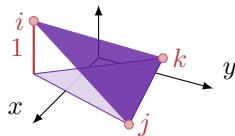
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$$W_{\alpha_{1i}} = \begin{vmatrix} 1 & x_i & y_i \\ 0 & x_j & y_j \\ 0 & x_k & y_k \end{vmatrix} = x_j y_k - x_k y_j$$



$N_i(x^e, y^e)$



# Determination of shape functions for 3-node element

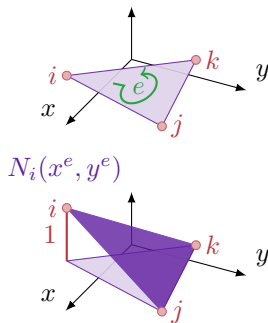
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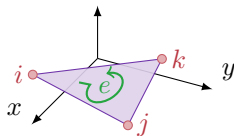
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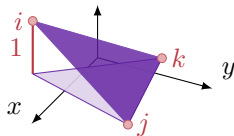
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$N_i(x^e, y^e)$



$$\alpha_{1i} = \frac{x_j y_k - x_k y_j}{2P_{\Delta}}$$

# Determination of shape functions for 3-node element

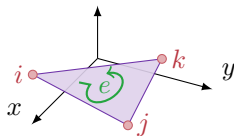
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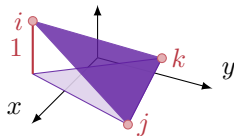
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$N_i(x^e, y^e)$



$$\alpha_{1i} = \frac{x_j y_k - x_k y_j}{2P_{\Delta}}$$

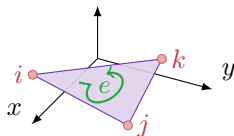
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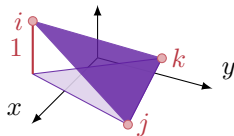
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$N_i(x^e, y^e)$



$$\alpha_{1i} = \frac{x_j y_k - x_k y_j}{2P_{\Delta}}$$

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# Determination of shape functions for 3-node element

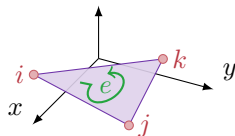
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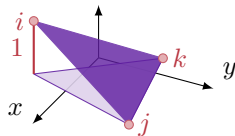
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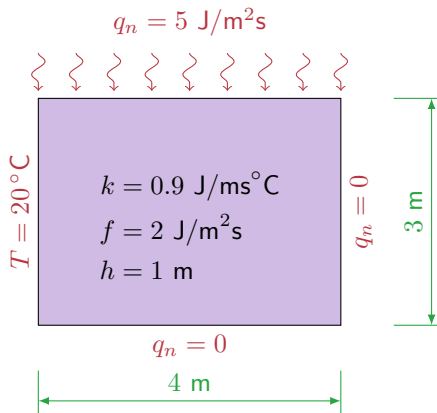
$N_i(x^e, y^e)$



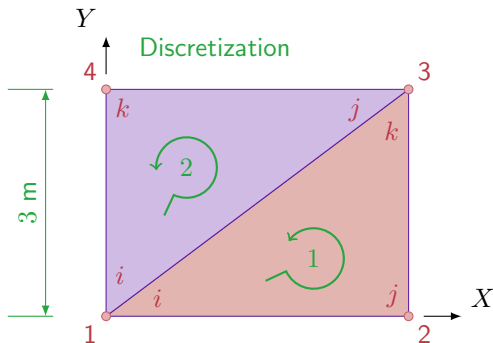
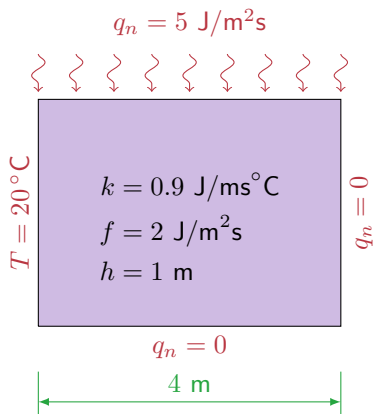
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## 2D example of heat flow – 3-node elements



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# Heat flow in 2D

$$\int_A (\nabla w)^T \mathbf{D}h \nabla T dA = - \int_{\Gamma_q} wh\hat{q}d\Gamma - \int_{\Gamma_T} whq_n d\Gamma + \int_A whfdA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

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$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}\mathbf{w} = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

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$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\mathbf{w}^T \int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \mathbf{w}^T \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \mathbf{w}^T \int_A \mathbf{N}^T f dA, \quad \forall \mathbf{w}$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

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$$\int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \int_A \mathbf{N}^T f dA$$

$$\mathbf{K} = \int_A \mathbf{B}^T k \mathbf{B} dA, \quad \mathbf{f} = \int_A \mathbf{N}^T f dA, \quad \mathbf{f}_b = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma$$

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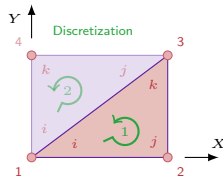
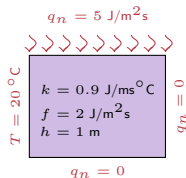
$$\mathbf{K} = \int_A \mathbf{B}^T k \mathbf{B} dA, \quad \mathbf{f} = \int_A \mathbf{N}^T f dA, \quad \mathbf{f}_b = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma$$

$$\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$$

# 2D example of heat flow – 3-node elements

## K matrix – element 1

$$\mathbf{N}^1 = \left[ 1 - \frac{1}{4}x \quad \frac{1}{4}x - \frac{1}{3}y \quad \frac{1}{3}y \right]$$

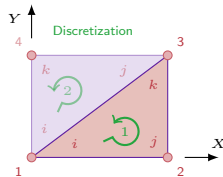
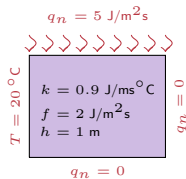


# 2D example of heat flow – 3-node elements

**K** matrix – element 1

$$\mathbf{N}^1 = \left[ 1 - \frac{1}{4}x \quad \frac{1}{4}x - \frac{1}{3}y \quad \frac{1}{3}y \right]$$

$$\mathbf{B}^1 = \nabla \mathbf{N} = \begin{bmatrix} -0.250 & 0.250 & 0.000 \\ 0.000 & -0.333 & 0.333 \end{bmatrix}$$



# 2D example of heat flow – 3-node elements

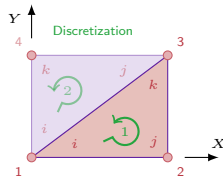
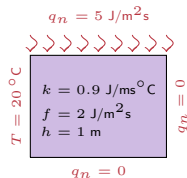
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$$\mathbf{B}^1 = \nabla \mathbf{N} = \begin{bmatrix} -0.250 & 0.250 & 0.000 \\ 0.000 & -0.333 & 0.333 \end{bmatrix}$$

$$\mathbf{K}^1 = \int_{A^1} \mathbf{B}^T k \mathbf{B} dA = A^1 \mathbf{B}^T k \mathbf{B}$$

$$= \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

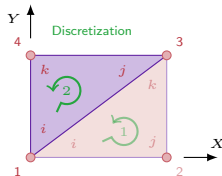
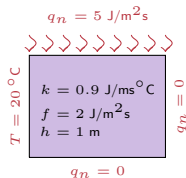


# 2D example of heat flow – 3-node elements

## K matrix – element 2

$$\mathbf{N}^2 = \left[ 1 - \frac{1}{3}y \quad \frac{1}{4}x \quad \frac{1}{3}y - \frac{1}{4}x \right]$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$



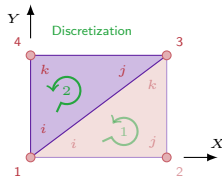
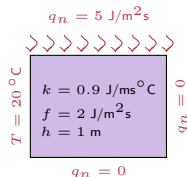
# 2D example of heat flow – 3-node elements

## K matrix – element 2

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$$\mathbf{B}^2 = \nabla \mathbf{N} = \begin{bmatrix} 0.000 & 0.250 & -0.250 \\ -0.333 & 0.000 & 0.333 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$



# 2D example of heat flow – 3-node elements

## K matrix – element 2

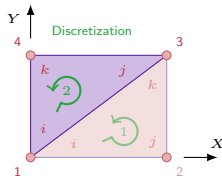
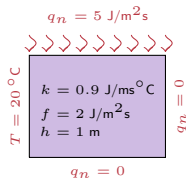
$$\mathbf{N}^2 = \left[ 1 - \frac{1}{3}y \quad \frac{1}{4}x \quad \frac{1}{3}y - \frac{1}{4}x \right]$$

$$\mathbf{B}^2 = \nabla \mathbf{N} = \begin{bmatrix} 0.000 & 0.250 & -0.250 \\ -0.333 & 0.000 & 0.333 \end{bmatrix}$$

$$\mathbf{K}^2 = \int_{A^2} \mathbf{B}^T k \mathbf{B} dA = A^2 \mathbf{B}^T k \mathbf{B}$$

$$= \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$





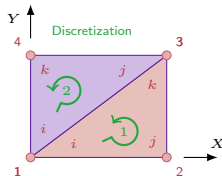
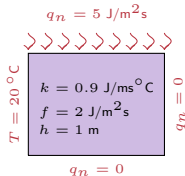
# 2D example of heat flow – 3-node elements

$\mathbf{f}$  vector – element 1 and 2 -  $A^1 = A^2$

$$\mathbf{f}^e = \int_{A^e} \mathbf{N}^T f dA = \frac{f}{3} A^e \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$



# 2D example of heat flow – 3-node elements

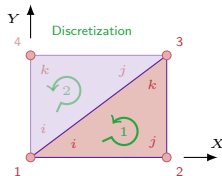
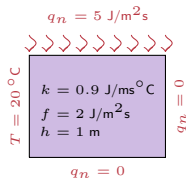
## $\mathbf{f}_b$ vector – element 1

$$\mathbf{f}_b^1 = - \int_{\Gamma_{ij}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{jk}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{ki}^1} (\mathbf{N}^1)^T q_n d\Gamma$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$



# 2D example of heat flow – 3-node elements

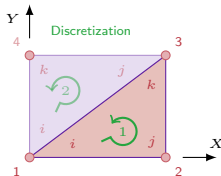
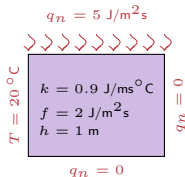
$\mathbf{f}_b$  vector – element 1

$$\mathbf{f}_b^1 = - \int_{\Gamma_{ij}^1} (\mathbf{N}^1)^T \overset{b.c. = 0}{q_n} d\Gamma - \int_{\Gamma_{jk}^1} (\mathbf{N}^1)^T \overset{b.c. = 0}{q_n} d\Gamma$$

flow continuity  
along edge 1-3

$$q_{n_{ki}}^1 = -q_{n_{ij}}^2$$

$$- \int_{\Gamma_{ki}^1} (\mathbf{N}^1)^T q_n d\Gamma$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## $\mathbf{f}_b$ vector – element 1

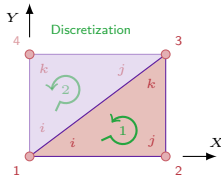
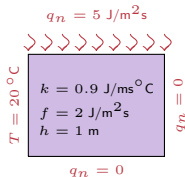
$$\mathbf{f}_b^1 = - \int_{\Gamma_{ij}^1} (\mathbf{N}^1)^T \overset{b.c. = 0}{q_n} d\Gamma - \int_{\Gamma_{jk}^1} (\mathbf{N}^1)^T \overset{b.c. = 0}{q_n} d\Gamma$$

flow continuity  
along edge 1-3

$$q_{n_{ki}}^1 = -q_{n_{ij}}^2$$

$$- \int_{\Gamma_{ki}^1} (\mathbf{N}^1)^T q_n d\Gamma$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

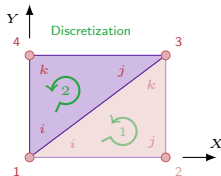
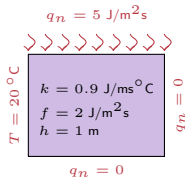
$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## $\mathbf{f}_b$ vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{ij}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$- \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{ki}^2} (\mathbf{N}^2)^T q_n d\Gamma$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

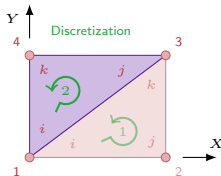
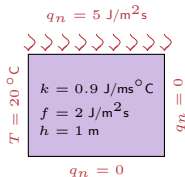
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix},$$

# 2D example of heat flow – 3-node elements

## $\mathbf{f}_b$ vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{ij}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{ki}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

flow continuity  
along edge 1-3  
 $q_{n_{ki}}^1 = -q_{n_{ij}}^2$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix},$$

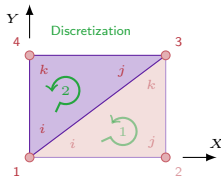
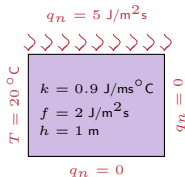
# 2D example of heat flow – 3-node elements

$\mathbf{f}_b$  vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{ki}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$- \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma = - \int_0^4 (\mathbf{N}^2(x, y=3))^T (-5) dx$$

$$= \begin{bmatrix} 0 \\ 10 \\ 10 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

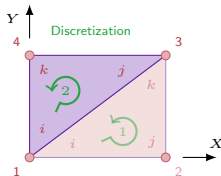
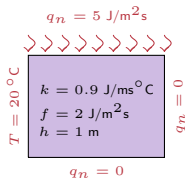
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix},$$

# 2D example of heat flow – 3-node elements

$\mathbf{f}_b$  vector – element 2

$$\mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 10 \\ 10 \end{bmatrix} - \int_{\Gamma_{ki}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$\begin{aligned} - \int_{\Gamma_{ki}^2} (\mathbf{N}^2)^T q_n d\Gamma &= - \int_0^3 (\mathbf{N}^2(x=0, y))^T q_n dx \\ &= \begin{bmatrix} f_{b1} \\ 0 \\ f_{b4} \end{bmatrix} \end{aligned}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix},$$

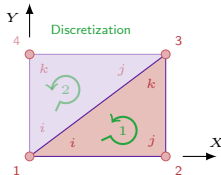
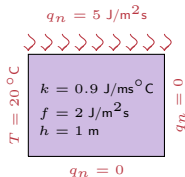


# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.338 & -0.338 & 0.000 & 0.000 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.600 & 0.000 \\ 0.000 & 0.000 & 0.000 & 0.000 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

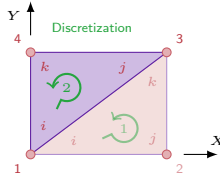
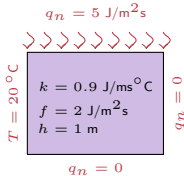
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

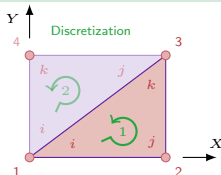
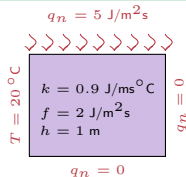
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{f}^1 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 4 \\ 4 \\ 4 \\ 0 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

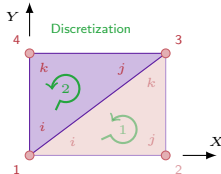
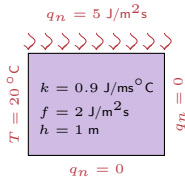
$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{f}^1 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix} \quad \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

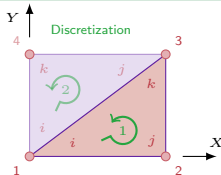
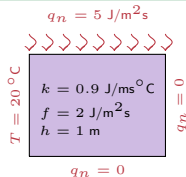
# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$



$$\mathbf{f}_b = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

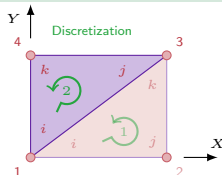
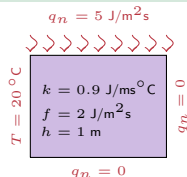
$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Assembly

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

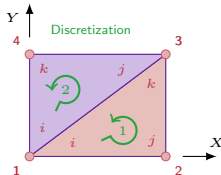
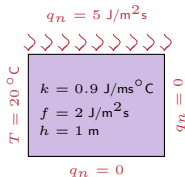
$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

$$\begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix} \begin{bmatrix} \Theta_1 \\ \Theta_2 \\ \Theta_3 \\ \Theta_4 \end{bmatrix} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

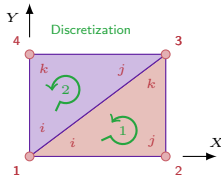
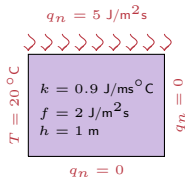
$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

$$\begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix} \begin{bmatrix} 20 \\ \Theta_2 \\ \Theta_3 \\ 20 \end{bmatrix} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

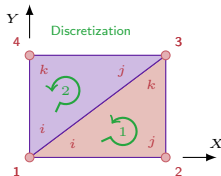
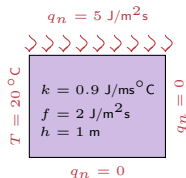


# 2D example of heat flow – 3-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

$$\begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix} \begin{bmatrix} 20 \\ \Theta_2 \\ \Theta_3 \\ 20 \end{bmatrix} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

**Solution:**  $\Theta_2 = 48.040$ ,  $\Theta_3 = 57.145$ ,  
 $f_{b1} = -17.463$ ,  $f_{b4} = -26.537$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

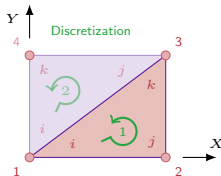
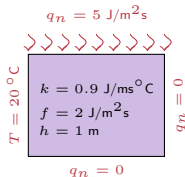
$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Heat flux vector – element 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

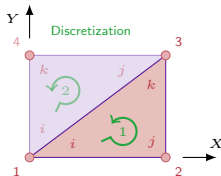
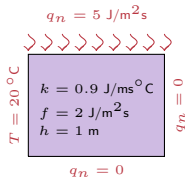
$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Heat flux vector – element 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix}$$

$$\begin{aligned} \mathbf{q}^1 &= -k\mathbf{B}^1\Theta^1 \\ &= -0.9 \begin{bmatrix} -0.250 & 0.250 & 0.000 \\ 0.000 & -0.333 & 0.333 \end{bmatrix} \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix} \\ &= \begin{bmatrix} -6.309 \\ -2.732 \end{bmatrix} \end{aligned}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

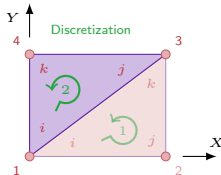
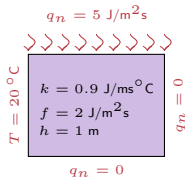
$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Heat flux vector – element 2

$$\Theta^2 = \begin{bmatrix} 20 \\ 57.145 \\ 20 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

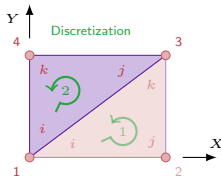
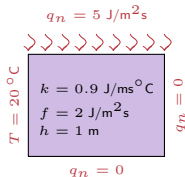
$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Heat flux vector – element 2

$$\Theta^2 = \begin{bmatrix} 20 \\ 57.145 \\ 20 \end{bmatrix}$$

$$\begin{aligned} \mathbf{q}^2 &= -k\mathbf{B}^2\Theta^2 \\ &= -0.9 \begin{bmatrix} 0.000 & 0.250 & -0.250 \\ -0.333 & 0.000 & 0.333 \end{bmatrix} \begin{bmatrix} 20 \\ 57.145 \\ 20 \end{bmatrix} \\ &= \begin{bmatrix} -8.358 \\ 0.000 \end{bmatrix} \end{aligned}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

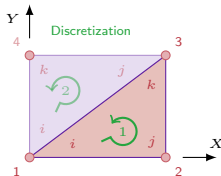
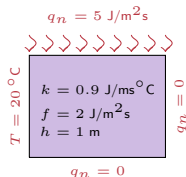
$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

## Computation of temperature at a point in el. 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix}$$

$$T^e(x^e, y^e) = \mathbf{N}^e(x^e, y^e) \Theta^e$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

# 2D example of heat flow – 3-node elements

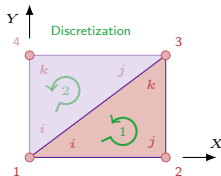
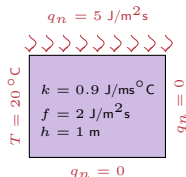
## Computation of temperature at a point in el. 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix}$$

$$T^e(x^e, y^e) = \mathbf{N}^e(x^e, y^e) \Theta^e$$

e.g. at centre of mass  $(\frac{8}{3}, 1)$

$$T^1\left(\frac{8}{3}, 1\right) = \begin{bmatrix} 1 - \frac{1}{4} \cdot \frac{8}{3} & \frac{1}{4} \cdot \frac{8}{3} - \frac{1}{3} \cdot 1 & \frac{1}{3} \cdot 1 \end{bmatrix} \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \end{bmatrix} = 41.728$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.338 & -0.338 & 0.000 \\ -0.388 & 0.938 & -0.600 \\ 0.000 & -0.600 & 0.600 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.600 & 0.000 & -0.600 \\ 0.000 & 0.338 & -0.338 \\ -0.600 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 4 \\ 4 \\ 4 \end{bmatrix}$$

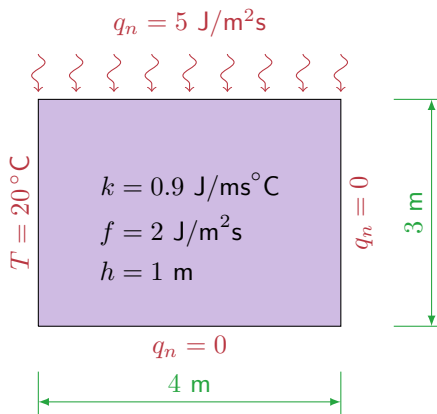
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} f_{b1} \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} 0.938 & -0.338 & 0.000 & -0.600 \\ -0.388 & 0.938 & -0.600 & 0.000 \\ 0.000 & -0.600 & 0.938 & -0.338 \\ -0.600 & 0.000 & -0.338 & 0.938 \end{bmatrix}$$

$$\mathbf{f} = \begin{bmatrix} 8 \\ 4 \\ 8 \\ 4 \end{bmatrix}, \quad \mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 10 \\ f_{b4} + 10 \end{bmatrix}$$

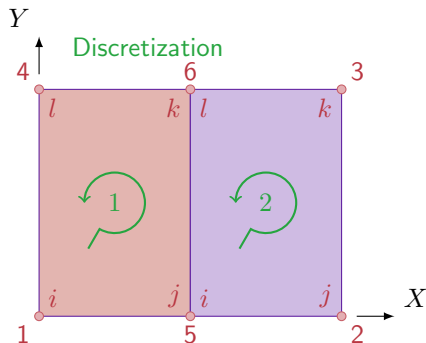
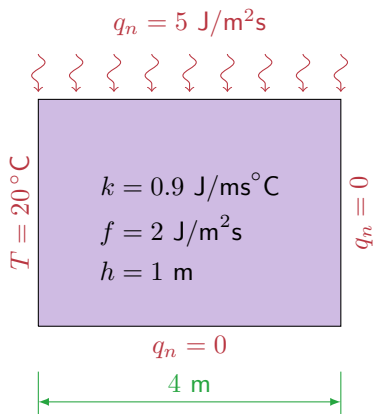
$$\Theta = \begin{bmatrix} 20 \\ 48.040 \\ 57.145 \\ 20 \end{bmatrix}$$

## 2D example of heat flow – 4-node elements





## 2D example of heat flow – 4-node elements



# Heat flow in 2D

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma_q} w h \hat{q} d\Gamma - \int_{\Gamma_T} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}\mathbf{w} = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}\mathbf{w} = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\mathbf{w}^T \int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \mathbf{w}^T \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \mathbf{w}^T \int_A \mathbf{N}^T f dA, \quad \forall \mathbf{w}$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}\mathbf{w} = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \int_A \mathbf{N}^T f dA$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}\mathbf{w} = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \int_A \mathbf{N}^T f dA$$

$$\mathbf{K} = \int_A \mathbf{B}^T k \mathbf{B} dA, \quad \mathbf{f} = \int_A \mathbf{N}^T f dA, \quad \mathbf{f}_b = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma$$

$$\int_A (\nabla w)^T \mathbf{D} h \nabla T dA = - \int_{\Gamma} w h q_n d\Gamma + \int_A w h f dA$$

+ boundary condition

$$T = \hat{T} \quad \text{on } \Gamma_T$$

$$T = \mathbf{N}\Theta, \quad w = \mathbf{N}w = \mathbf{w}^T \mathbf{N}^T, \quad \nabla T = \mathbf{B}\Theta$$

$$\nabla w = \mathbf{w}^T \mathbf{B}^T, \quad \mathbf{D} = k\mathbf{I}, \quad h = \text{const}$$

$$\int_A \mathbf{B}^T k \mathbf{B} dA \Theta = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma + \int_A \mathbf{N}^T f dA$$

$$\mathbf{K} = \int_A \mathbf{B}^T k \mathbf{B} dA, \quad \mathbf{f} = \int_A \mathbf{N}^T f dA, \quad \mathbf{f}_b = - \int_{\Gamma} \mathbf{N}^T q_n d\Gamma$$

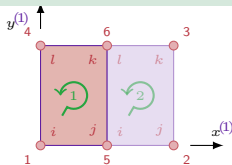
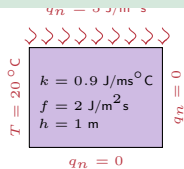
$$\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$$



# 2D example of heat flow – 4-node elements

## K matrix – element 1

$$\mathbf{N}^1 = \begin{bmatrix} \frac{(x^{(1)}-2)(y^{(1)}-3)}{2 \cdot 3} & \frac{x^{(1)}(y^{(1)}-3)}{-2 \cdot 3} & \frac{x^{(1)}y^{(1)}}{2 \cdot 3} & \frac{(x^{(1)}-2)y^{(1)}}{-2 \cdot 3} \end{bmatrix}$$

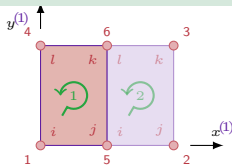
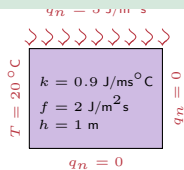


# 2D example of heat flow – 4-node elements

## K matrix – element 1

$$\mathbf{N}^1 = \begin{bmatrix} \frac{(x^{(1)}-2)(y^{(1)}-3)}{2 \cdot 3} & \frac{x^{(1)}(y^{(1)}-3)}{-2 \cdot 3} & \frac{x^{(1)}y^{(1)}}{2 \cdot 3} & \frac{(x^{(1)}-2)y^{(1)}}{-2 \cdot 3} \end{bmatrix}$$

$$\mathbf{B}^1 = \nabla \mathbf{N}^1 = \begin{bmatrix} \frac{y^{(1)}-3}{6} & \frac{y^{(1)}-3}{-6} & \frac{y^{(1)}}{6} & \frac{y^{(1)}}{-6} \\ \frac{x^{(1)}-2}{6} & \frac{x^{(1)}}{-6} & \frac{x^{(1)}}{6} & \frac{x^{(1)}-2}{-6} \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

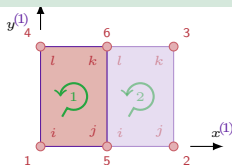
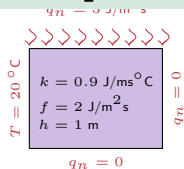
## K matrix – element 1

$$\mathbf{N}^1 = \begin{bmatrix} \frac{(x^{(1)}-2)(y^{(1)}-3)}{2 \cdot 3} & \frac{x^{(1)}(y^{(1)}-3)}{-2 \cdot 3} & \frac{x^{(1)}y^{(1)}}{2 \cdot 3} & \frac{(x^{(1)}-2)y^{(1)}}{-2 \cdot 3} \end{bmatrix}$$

$$\mathbf{B}^1 = \nabla \mathbf{N}^1 = \begin{bmatrix} \frac{y^{(1)}-3}{6} & \frac{y^{(1)}-3}{-6} & \frac{y^{(1)}}{6} & \frac{y^{(1)}}{-6} \\ \frac{x^{(1)}-2}{6} & \frac{x^{(1)}}{-6} & \frac{x^{(1)}}{6} & \frac{x^{(1)}-2}{-6} \end{bmatrix}$$

$$\mathbf{K}^1 = \int_{A^1} \mathbf{B}^T k \mathbf{B} dA = \int_0^3 \int_0^2 \mathbf{B}^T k \mathbf{B} dx^{(1)} dy^{(1)} =$$

$$= \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

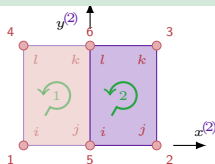
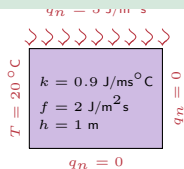


# 2D example of heat flow – 4-node elements

## K matrix – element 2

$$\mathbf{N}^2 = \begin{bmatrix} \frac{(x^{(2)}-2)(y^{(2)}-3)}{2 \cdot 3} & \frac{x^{(2)}(y^{(2)}-3)}{-2 \cdot 3} & \frac{x^{(2)}y^{(2)}}{2 \cdot 3} & \frac{(x^{(2)}-2)y^{(2)}}{-2 \cdot 3} \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$



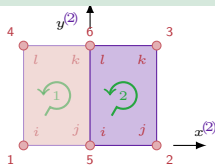
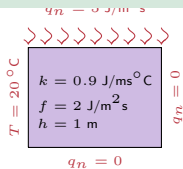
# 2D example of heat flow – 4-node elements

## K matrix – element 2

$$\mathbf{N}^2 = \begin{bmatrix} \frac{(x^{(2)}-2)(y^{(2)}-3)}{2 \cdot 3} & \frac{x^{(2)}(y^{(2)}-3)}{-2 \cdot 3} & \frac{x^{(2)}y^{(2)}}{2 \cdot 3} & \frac{(x^{(2)}-2)y^{(2)}}{-2 \cdot 3} \end{bmatrix}$$

$$\mathbf{B}^2 = \nabla \mathbf{N}^2 = \begin{bmatrix} \frac{y^{(2)}-3}{6} & \frac{y^{(2)}-3}{-6} & \frac{y^{(2)}}{6} & \frac{y^{(2)}}{-6} \\ \frac{x^{(2)}-2}{6} & \frac{x^{(2)}}{-6} & \frac{x^{(2)}}{6} & \frac{x^{(2)}-2}{-6} \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

## K matrix – element 2

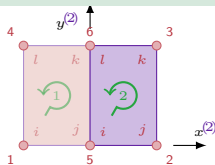
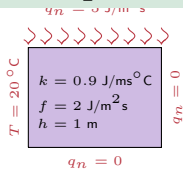
$$\mathbf{N}^2 = \begin{bmatrix} \frac{(x^{(2)}-2)(y^{(2)}-3)}{2 \cdot 3} & \frac{x^{(2)}(y^{(2)}-3)}{-2 \cdot 3} & \frac{x^{(2)}y^{(2)}}{2 \cdot 3} & \frac{(x^{(2)}-2)y^{(2)}}{-2 \cdot 3} \end{bmatrix}$$

$$\mathbf{B}^2 = \nabla \mathbf{N}^2 = \begin{bmatrix} \frac{y^{(2)}-3}{6} & \frac{y^{(2)}-3}{-6} & \frac{y^{(2)}}{6} & \frac{y^{(2)}}{-6} \\ \frac{x^{(2)}-2}{6} & \frac{x^{(2)}-2}{-6} & \frac{x^{(2)}}{6} & \frac{x^{(2)}-2}{-6} \end{bmatrix}$$

$$\mathbf{K}^2 = \int_{A^2} \mathbf{B}^T k \mathbf{B} dA = \int_0^3 \int_0^2 \mathbf{B}^T k \mathbf{B} dx^{(2)} dy^{(2)} =$$

$$= \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$



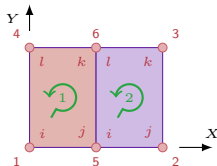
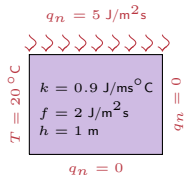
# 2D example of heat flow – 4-node elements

$f$  vector – element 1 and 2 -  $A^1 = A^2$

$$\mathbf{f}^e = \int_{A^e} \mathbf{N}^T f dA = \frac{f}{4} A^e \begin{bmatrix} 1 \\ 1 \\ 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

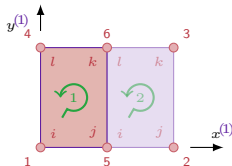
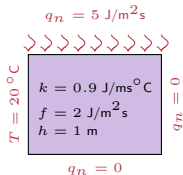
## $\mathbf{f}_b$ vector – element 1

$$\mathbf{f}_b^1 = - \int_{\Gamma_{ij}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{jk}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{kl}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$



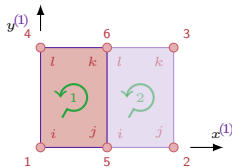
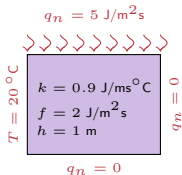


# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 1

$$\mathbf{f}_b^1 = - \int_{\Gamma_{ij}^1} (\mathbf{N}^1)^T \overset{\text{b.c.} = 0}{q_n} d\Gamma - \int_{\Gamma_{jk}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{kl}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma$$

flow continuity  
along edge 5-6  
 $q_{nj}^1 = -q_{nl}^2$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

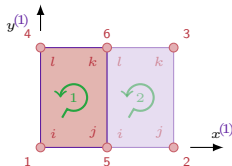
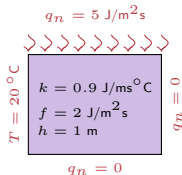
$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

$\mathbf{f}_b$  vector – element 1

$$\mathbf{f}_b^1 = - \int_{\Gamma_{kl}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

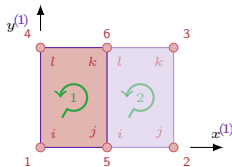
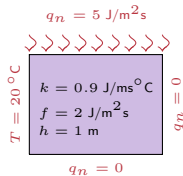
$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 1

$$\begin{aligned} \mathbf{f}_b^1 &= - \int_{\Gamma_{kl}^1} (\mathbf{N}^1)^T q_n d\Gamma - \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma \\ &- \int_{\Gamma_{kl}^1} (\mathbf{N}^1)^T q_n d\Gamma = - \int_0^2 (\mathbf{N}^1(x^{(1)}, y^{(1)}=3))^T (-5) dx^{(1)} \\ &= \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix} \end{aligned}$$



$$\begin{aligned} \mathbf{K}^1 &= \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix} \\ \mathbf{K}^2 &= \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix} \\ \mathbf{f}^1 &= \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix} \end{aligned}$$

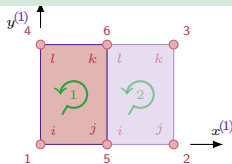
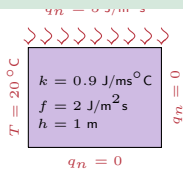
# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 1

$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix} - \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma$$

$$- \int_{\Gamma_{li}^1} (\mathbf{N}^1)^T q_n d\Gamma = - \int_0^3 (\mathbf{N}^1(x^{(1)}=0, y^{(1)}))^T q_n dy^{(1)}$$

$$= \begin{bmatrix} f_{b1} \\ 0 \\ 0 \\ f_{b4} \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

$\mathbf{f}_b$  vector – element 1

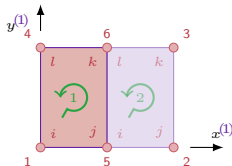
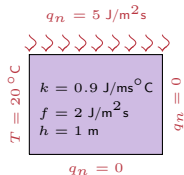
$$\mathbf{f}_b^1 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 0 \\ f_{b4} \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 2

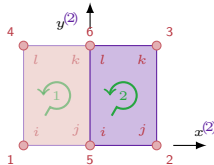
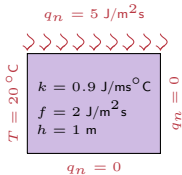
$$\mathbf{f}_b^2 = - \int_{\Gamma_{ij}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{kl}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{li}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix},$$



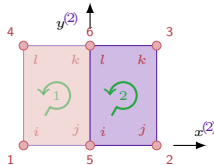
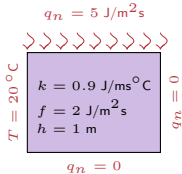
# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{ij}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{jk}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$- \int_{\Gamma_{kl}^2} (\mathbf{N}^2)^T q_n d\Gamma - \int_{\Gamma_{li}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

flow continuity  
along edge 5-6  
 $q_{n,jk}^1 = -q_{n,li}^2$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

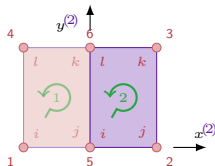
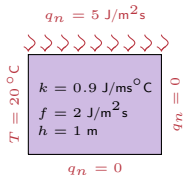
$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix},$$

# 2D example of heat flow – 4-node elements

$\mathbf{f}_b$  vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{kl}^2} (\mathbf{N}^2)^T q_n d\Gamma$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix},$$

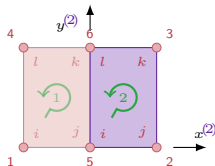
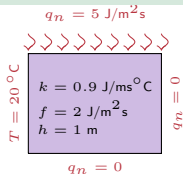


# 2D example of heat flow – 4-node elements

## $\mathbf{f}_b$ vector – element 2

$$\mathbf{f}_b^2 = - \int_{\Gamma_{kl}^2} (\mathbf{N}^2)^T q_n d\Gamma$$

$$\begin{aligned}
 - \int_{\Gamma_{kl}^2} (\mathbf{N}^2)^T q_n d\Gamma &= - \int_0^2 (\mathbf{N}^1(x^{(2)}, y^{(2)}=3))^T (-5) dx^{(2)} \\
 &= \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}
 \end{aligned}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

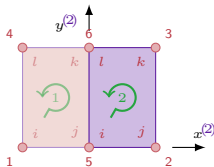
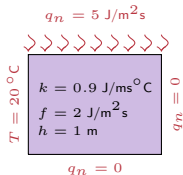
$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix},$$

# 2D example of heat flow – 4-node elements

$\mathbf{f}_b$  vector – element 2

$$\mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

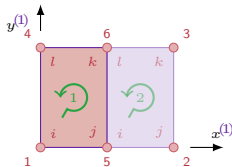
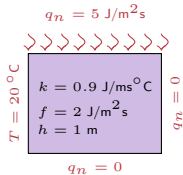
$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix},$$

# 2D example of heat flow – 4-node elements

## Assembly

$$K^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix} \begin{matrix} \textcircled{1} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{4} \end{matrix}$$

$$K = \begin{bmatrix} 0.650 & 0.000 & 0.000 & 0.025 & -0.350 & -0.325 \\ 0.000 & 0.000 & 0.000 & 0.000 & 0.000 & 0.000 \\ 0.000 & 0.000 & 0.000 & 0.000 & 0.000 & 0.000 \\ 0.025 & 0.000 & 0.000 & 0.650 & -0.325 & -0.350 \\ -0.350 & 0.000 & 0.000 & -0.325 & 0.650 & 0.025 \\ -0.325 & 0.000 & 0.000 & -0.350 & 0.025 & 0.650 \end{bmatrix}$$



$$K^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$K^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$f^1 = f^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$f_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad f_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

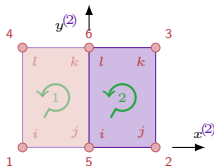
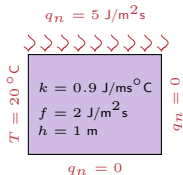
# 2D example of heat flow – 4-node elements

## Assembly

$$K^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

(5)
(2)
(3)
(6)

$$K = \begin{bmatrix} 0.650 & 0.000 & 0.000 & 0.025 & -0.350 & -0.325 \\ 0.000 & 0.650 & 0.025 & 0.000 & -0.350 & -0.325 \\ 0.000 & 0.025 & 0.650 & 0.000 & -0.325 & -0.350 \\ 0.025 & 0.000 & 0.000 & 0.650 & -0.325 & -0.350 \\ -0.350 & -0.350 & -0.325 & -0.325 & 1.300 & 0.050 \\ -0.325 & -0.325 & -0.350 & -0.350 & 0.050 & 1.300 \end{bmatrix}$$



$$K^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$K^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$f^1 = f^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$f_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad f_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

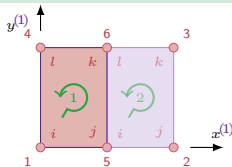
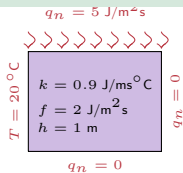
# 2D example of heat flow – 4-node elements

## Assembly

$$\mathbf{f}^1 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$



$$\mathbf{f} = \begin{bmatrix} 3 \\ 0 \\ 0 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

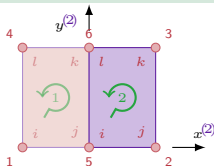
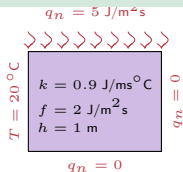
$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Assembly

$$\mathbf{f}^1 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix} \begin{matrix} \textcircled{1} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{4} \end{matrix} \qquad \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \end{bmatrix} \begin{matrix} \textcircled{5} \\ \textcircled{2} \\ \textcircled{6} \end{matrix}$$
$$\mathbf{f} = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \\ 6 \\ 6 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

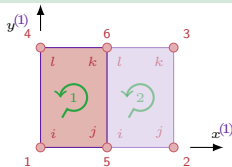
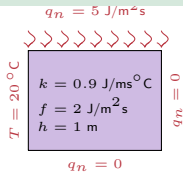
# 2D example of heat flow – 4-node elements

## Assembly

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix} \begin{matrix} \textcircled{1} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{4} \end{matrix}$$



$$\mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 0 \\ 5 + f_{b4} \\ 0 \\ 5 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Assembly

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix} \begin{matrix} \textcircled{1} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{4} \end{matrix}$$

$$\mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix} \begin{matrix} \textcircled{5} \\ \textcircled{2} \\ \textcircled{3} \\ \textcircled{6} \end{matrix}$$

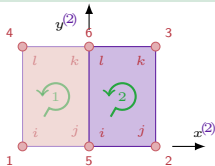
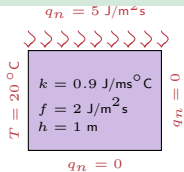
$$\mathbf{f}_b = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \\ 0 \\ 10 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$





# 2D example of heat flow – 4-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

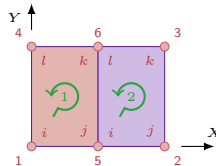
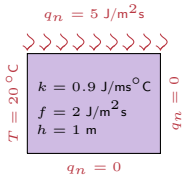
$$\begin{bmatrix} 0.650 & 0.000 & 0.000 & 0.025 & -0.350 & -0.325 \\ 0.000 & 0.650 & 0.025 & 0.000 & -0.350 & -0.325 \\ 0.000 & 0.025 & 0.650 & 0.000 & -0.325 & -0.350 \\ 0.025 & 0.000 & 0.000 & 0.650 & -0.325 & -0.350 \\ -0.350 & -0.350 & -0.325 & -0.325 & 1.300 & 0.050 \\ -0.325 & -0.325 & -0.350 & -0.350 & 0.050 & 1.300 \end{bmatrix} \begin{bmatrix} \Theta_1 \\ \Theta_2 \\ \Theta_3 \\ \Theta_4 \\ \Theta_5 \\ \Theta_6 \end{bmatrix} = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 6 \\ 6 \\ 6 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \\ 0 \\ 10 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

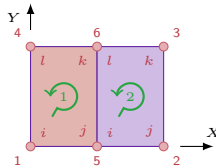
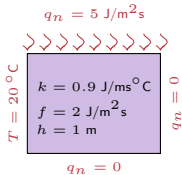
$$\begin{bmatrix} 0.650 & 0.000 & 0.000 & 0.025 & -0.350 & -0.325 \\ 0.000 & 0.650 & 0.025 & 0.000 & -0.350 & -0.325 \\ 0.000 & 0.025 & 0.650 & 0.000 & -0.325 & -0.350 \\ 0.025 & 0.000 & 0.000 & 0.650 & -0.325 & -0.350 \\ -0.350 & -0.350 & -0.325 & -0.325 & 1.300 & 0.050 \\ -0.325 & -0.325 & -0.350 & -0.350 & 0.050 & 1.300 \end{bmatrix} \begin{bmatrix} 20 \\ \Theta_2 \\ \Theta_3 \\ 20 \\ \Theta_5 \\ \Theta_6 \end{bmatrix} = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 6 \\ 6 \\ 6 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \\ 0 \\ 10 \end{bmatrix}$$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

FEM equation set:  $\mathbf{K}\Theta = \mathbf{f} + \mathbf{f}_b$

$$\begin{bmatrix} 0.650 & 0.000 & 0.000 & 0.025 & -0.350 & -0.325 \\ 0.000 & 0.650 & 0.025 & 0.000 & -0.350 & -0.325 \\ 0.000 & 0.025 & 0.650 & 0.000 & -0.325 & -0.350 \\ 0.025 & 0.000 & 0.000 & 0.650 & -0.325 & -0.350 \\ -0.350 & -0.350 & -0.325 & -0.325 & 1.300 & 0.050 \\ -0.325 & -0.325 & -0.350 & -0.350 & 0.050 & 1.300 \end{bmatrix} \begin{bmatrix} \Theta_2 \\ \Theta_3 \\ \Theta_3 \\ \Theta_5 \\ \Theta_6 \\ \Theta_6 \end{bmatrix} = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 6 \\ 6 \\ 6 \end{bmatrix} + \begin{bmatrix} f_{b1} \\ 0 \\ 5 + f_{b4} \\ 0 \\ 10 \end{bmatrix}$$

**Solution:**  $\Theta_2 = 48.429$ ,  $\Theta_3 = 56.756$ ,  $\Theta_5 = 40.361$ ,  $\Theta_6 = 48.528$ ,

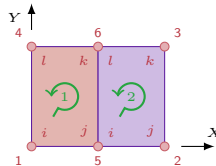
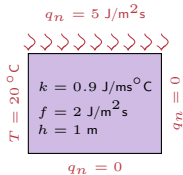
$f_{b1} = -19.398$ ,  $f_{b4} = -24.602$

$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

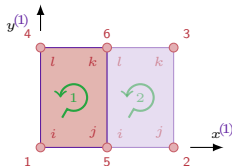
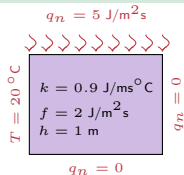
$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

## Heat flux vector – element 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Heat flux vector – element 1

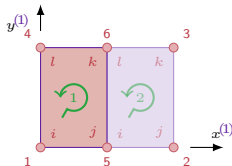
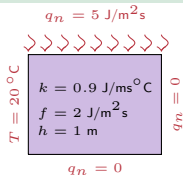
$$\Theta^1 = \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$

$$\mathbf{q}^1 = -k\mathbf{B}^1\Theta^1$$

$$= -0.9 \begin{bmatrix} \frac{y^{(1)}-3}{6} & \frac{y^{(1)}-3}{-6} & \frac{y^{(1)}}{6} & \frac{y^{(1)}}{-6} \\ \frac{x^{(1)}-2}{6} & \frac{x^{(1)}}{-6} & \frac{x^{(1)}}{6} & \frac{x^{(1)}-2}{-6} \end{bmatrix} \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$

$$= \begin{bmatrix} -1.225y - 9.192 \\ -1.225x \end{bmatrix}$$

e.g. at centre of mass  $\mathbf{q}^1(1, 1.5) = \begin{bmatrix} -11.000 \\ -1.225 \end{bmatrix}$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

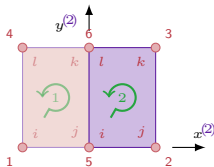
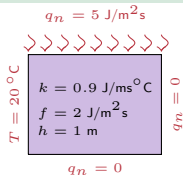
$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Heat flux vector – element 2

$$\Theta^2 = \begin{bmatrix} 40.361 \\ 48.429 \\ 56.756 \\ 48.528 \end{bmatrix}$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Heat flux vector – element 2

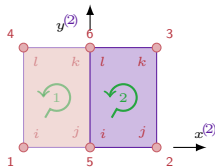
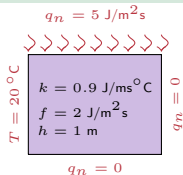
$$\Theta^2 = \begin{bmatrix} 40.361 \\ 48.429 \\ 56.756 \\ 48.528 \end{bmatrix}$$

$$\mathbf{q}^2 = -k\mathbf{B}^2\Theta^2$$

$$= -0.9 \begin{bmatrix} \frac{y^{(2)}-3}{6} & \frac{y^{(2)}-3}{-6} & \frac{y^{(2)}}{6} & \frac{y^{(2)}}{-6} \\ \frac{x^{(2)}-2}{6} & \frac{x^{(2)}}{-6} & \frac{x^{(2)}}{6} & \frac{x^{(2)}-2}{-6} \end{bmatrix} \begin{bmatrix} 40.361 \\ 48.429 \\ 56.756 \\ 48.528 \end{bmatrix}$$

$$= \begin{bmatrix} -0.024y - 3.631 \\ -0.024x - 2.450 \end{bmatrix}$$

e.g. at centre of mass  $\mathbf{q}^2(1, 1.5) = \begin{bmatrix} -3.667 \\ -2.474 \end{bmatrix}$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

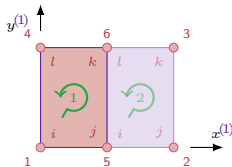
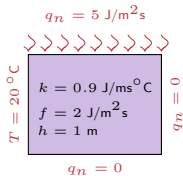
$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$

# 2D example of heat flow – 4-node elements

## Computation of temperature at a point in el. 1

$$\Theta^1 = \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$

$$T^e(x^e, y^e) = \mathbf{N}^e(x^e, y^e) \Theta^e$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$



# 2D example of heat flow – 4-node elements

## Computation of temperature at a point in el. 1

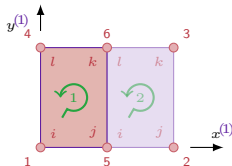
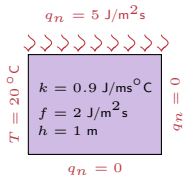
$$\Theta^1 = \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$

$$T^e(x^e, y^e) = \mathbf{N}^e(x^e, y^e) \Theta^e$$

e.g. at centre of mass (1, 1.5)

$$T^1(1, 1.5) = \left[ \frac{(1-2)(1.5-3)}{6} \quad \frac{1(1.5-3)}{-6} \quad \frac{1 \cdot 1.5}{6} \quad \frac{(1-2)1.5}{-6} \right] \begin{bmatrix} 20 \\ 40.361 \\ 48.528 \\ 20 \end{bmatrix}$$

$$= 32.222$$



$$\mathbf{K}^1 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{K}^2 = \begin{bmatrix} 0.650 & -0.350 & -0.325 & 0.025 \\ -0.350 & 0.650 & 0.025 & -0.325 \\ -0.325 & 0.025 & 0.650 & -0.350 \\ 0.025 & -0.325 & -0.350 & 0.650 \end{bmatrix}$$

$$\mathbf{f}^1 = \mathbf{f}^2 = \begin{bmatrix} 3 \\ 3 \\ 3 \\ 3 \end{bmatrix}$$

$$\mathbf{f}_b^1 = \begin{bmatrix} f_{b1} \\ 0 \\ 5 \\ 5 + f_{b4} \end{bmatrix}, \quad \mathbf{f}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 5 \\ 5 \end{bmatrix}$$

$$\Theta = \begin{bmatrix} 20 \\ 48.429 \\ 56.756 \\ 20 \\ 40.361 \\ 48.528 \end{bmatrix}$$