

FEM for continuum statics

Piotr Pluciński

e-mail: Piotr.Plucinski@pk.edu.pl

Jerzy Pamin

e-mail: Jerzy.Pamin@pk.edu.pl

Chair for Computational Engineering

Faculty of Civil Engineering, Cracow University of Technology

URL: www.CCE.pk.edu.pl

Lecture contents

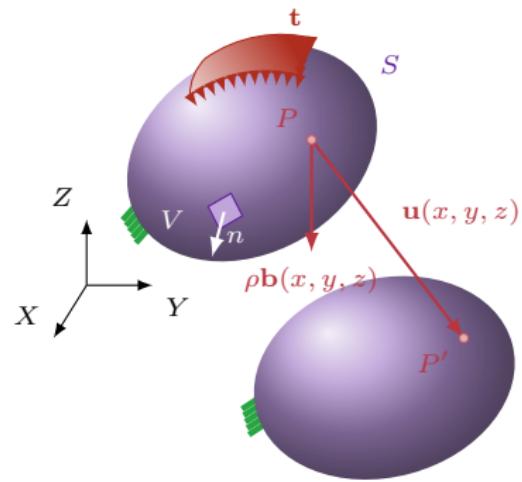
1 Equilibrium state

2 FEM discretization

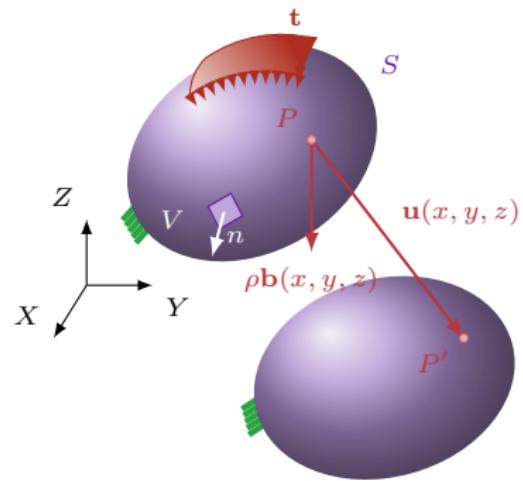
3 Plane stress

4 Example

Equilibrium state



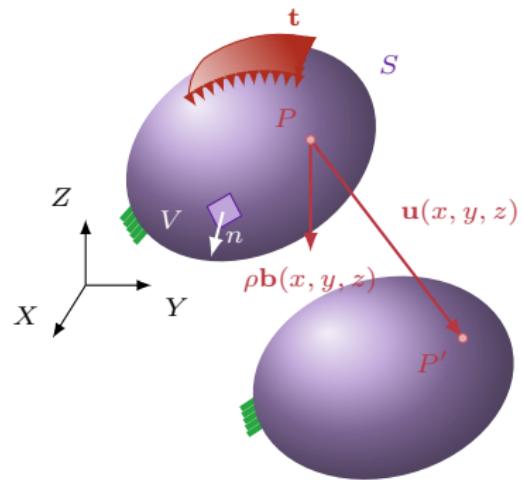
Equilibrium state



Body force density vector [N/m³]

$$\rho \mathbf{b} = \rho \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$$

Equilibrium state



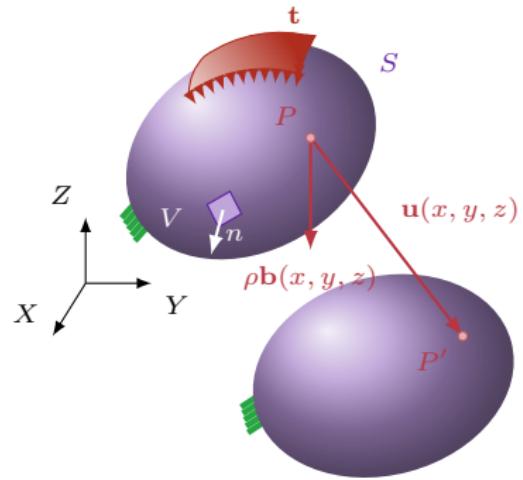
Body force density vector [N/m³]

$$\rho \mathbf{b} = \rho \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$$

Traction vector [N/m²]

$$\mathbf{t} = \begin{bmatrix} t_x \\ t_y \\ t_z \end{bmatrix}$$

Equilibrium state



Body force density vector [N/m³]

$$\rho \mathbf{b} = \rho \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$$

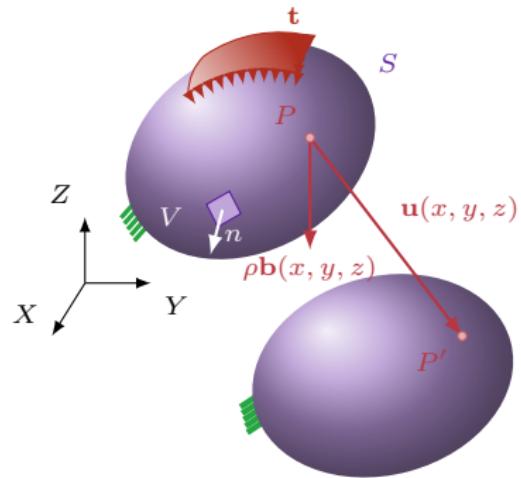
Traction vector [N/m²]

$$\mathbf{t} = \begin{bmatrix} t_x \\ t_y \\ t_z \end{bmatrix}$$

Displacement vector, strain tensor, stress tensor (Voigt's notation)

$$\mathbf{u} = \begin{bmatrix} u_x \\ u_y \\ u_z \end{bmatrix}, \quad \boldsymbol{\epsilon} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{xy} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{xz} & \epsilon_{yz} & \epsilon_{zz} \end{bmatrix} \rightarrow \begin{bmatrix} \epsilon_x \\ \epsilon_y \\ \epsilon_z \\ \gamma_{xy} \\ \gamma_{yz} \\ \gamma_{zx} \end{bmatrix}, \quad \boldsymbol{\sigma} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{xy} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{xz} & \sigma_{yz} & \sigma_{zz} \end{bmatrix} \rightarrow \begin{bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \tau_{xy} \\ \tau_{yz} \\ \tau_{zx} \end{bmatrix}$$

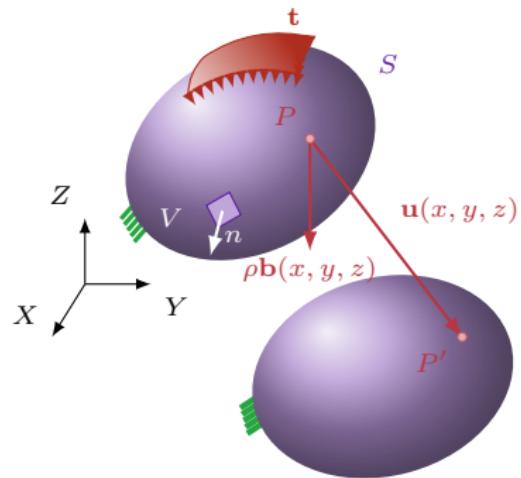
Equilibrium state



Equilibrium equations for a body

$$\int_S \mathbf{t} dS + \int_V \rho \mathbf{b} dV = 0$$

Equilibrium state



Equilibrium equations for a body

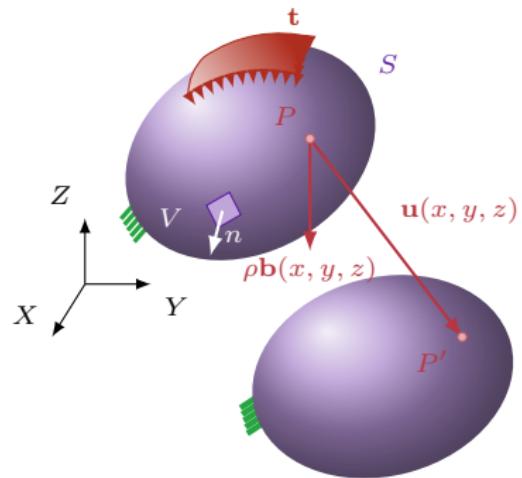
$$\int_S \mathbf{t} dS + \int_V \rho \mathbf{b} dV = 0$$

Static boundary conditions

$$\mathbf{t} = \sigma \mathbf{n}$$

where σ – stress tensor

Equilibrium state



Equilibrium equations for a body

$$\int_S \mathbf{t} dS + \int_V \rho \mathbf{b} dV = 0$$

Static boundary conditions

$$\mathbf{t} = \boldsymbol{\sigma} \mathbf{n}$$

where $\boldsymbol{\sigma}$ – stress tensor

Using Green–Gauss–Ostrogradsky theorem

$$\int_S \boldsymbol{\sigma} \mathbf{n} dS = \int_V \mathbf{L}^T \boldsymbol{\sigma} dV \quad \text{where } \mathbf{L} \text{ – differential operator matrix}$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation

$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation (complying with kinematic b.cs)

$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$
$$-\int_V (\mathbf{L} \delta \mathbf{u})^T \boldsymbol{\sigma} dV + \int_S (\delta \mathbf{u})^T \boldsymbol{\sigma} \mathbf{n} dS + \int_V (\delta \mathbf{u})^T \rho \mathbf{b} dV = 0$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation (complying with kinematic b.cs)

$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$
$$-\int_V (\mathbf{L} \delta \mathbf{u})^T \boldsymbol{\sigma} dV + \int_S (\delta \mathbf{u})^T \mathbf{\sigma n}^t dS + \int_V (\delta \mathbf{u})^T \rho \mathbf{b} dV = 0$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation (complying with kinematic b.cs)

$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$
$$-\int_V (\mathbf{L} \delta \mathbf{u})^T \boldsymbol{\sigma} dV + \int_S (\delta \mathbf{u})^T \mathbf{t} dS + \int_V (\delta \mathbf{u})^T \rho \mathbf{b} dV = 0$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$
$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation – it is virtual work principle

$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$

$$\int_V (\mathbf{L} \delta \mathbf{u})^T \boldsymbol{\sigma} dV = \int_S (\delta \mathbf{u})^T \mathbf{t} dS + \int_V (\delta \mathbf{u})^T \rho \mathbf{b} dV$$

Equilibrium equations

Navier's equations

$$\int_V (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \iff \mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b} = 0 \quad \forall P \in V$$

$$\sigma_{ij,j} + \rho b_i = 0$$

Weak formulation – weighting function $w \equiv \delta \mathbf{u}$ – kinematically admissible displacement variation – it is virtual work principle

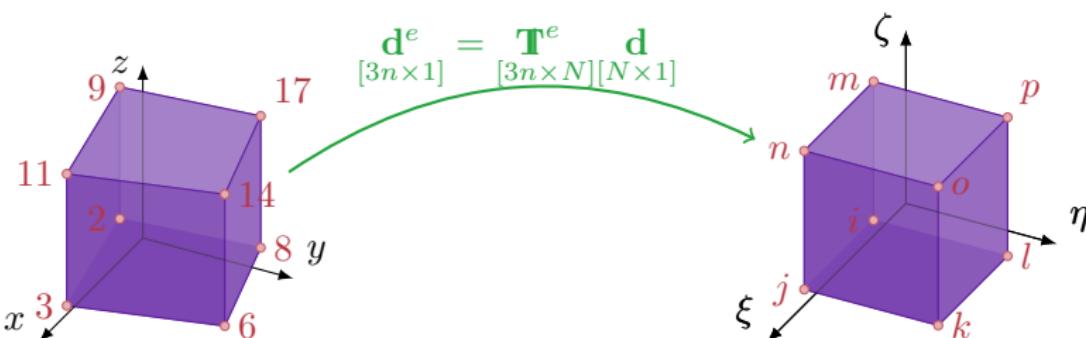
$$\int_V (\delta \mathbf{u})^T (\mathbf{L}^T \boldsymbol{\sigma} + \rho \mathbf{b}) dV = 0 \quad \forall \delta \mathbf{u}$$

FEM discretization (n =NNE, N =NDOF, E =NE)

Displacement field approximation

$$\mathbf{u}^{eh} = \sum_{i=1}^n N_i^e(\xi, \eta, \zeta) \mathbf{d}_i^e = \mathbf{N}^e \mathbf{d}^e$$

$$\mathbf{N}^e_{[3 \times 3n]} = \left[\begin{array}{ccc|c|ccc} N_1^e & 0 & 0 & \dots & N_n^e & 0 & 0 \\ 0 & N_1^e & 0 & \dots & 0 & N_n^e & 0 \\ 0 & 0 & N_1^e & \dots & 0 & 0 & N_n^e \end{array} \right] \quad \mathbf{d}^e_{[3n \times 1]} = \begin{bmatrix} \mathbf{d}_1^e \\ \vdots \\ \mathbf{d}_n^e \end{bmatrix}$$



$\mathbf{T}^e = \mathbf{T}^e \mathbf{B}^e$ – transformation matrix which defines topology (\mathbf{B}^e) and directional cosines of angles between the axes of global and local coordinate set (\mathbf{T}^e)

Equilibrium equation of discretized structure

Equilibrium equation ($\rho \mathbf{b}^e = \mathbf{f}^e$ – body force vector)

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \mathbf{N}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \mathbf{N}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\delta \mathbf{d}^e)^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\delta \mathbf{d}^e)^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$(\delta \mathbf{d})^T \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$(\delta \mathbf{d})^T \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$\forall \delta \mathbf{d}$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{L}^e \delta \mathbf{u}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\delta \mathbf{u}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\delta \mathbf{u}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \left\{ \int_{V^e} (\mathbf{B}^e \delta \mathbf{d}^e)^T \boldsymbol{\sigma}^e dV^e - \int_{S^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{t}^e dS^e - \int_{V^e} (\mathbf{N}^e \delta \mathbf{d}^e)^T \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E (\mathbf{T}^e \delta \mathbf{d})^T \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e - \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e - \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\} = 0$$

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

internal forces = external forces

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{V^e} \mathbf{B}^{e\text{T}} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{S^e} \mathbf{N}^{e\text{T}} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{e\text{T}} \mathbf{f}^e dV^e \right\}$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{V^e} \mathbf{B}^{e\text{T}} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{S^e} \mathbf{N}^{e\text{T}} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{e\text{T}} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d} dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \mathbf{D}^e \mathbf{B}^e dV^e \right\} \mathbf{T}^e \mathbf{d} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \bar{\mathbf{f}}^e dV^e \right\} \bar{\mathbf{p}}_b^e$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{V^e} \mathbf{B}^{e\text{T}} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{S^e} \mathbf{N}^{e\text{T}} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{e\text{T}} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{e\text{T}} \bar{\mathbf{K}}^e \mathbf{T}^e \mathbf{d} = \sum_{e=1}^E \mathbf{T}^{e\text{T}} \bar{\mathbf{p}}_b^e + \sum_{e=1}^E \mathbf{T}^{e\text{T}} \bar{\mathbf{p}}^e$$

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{V^e} \mathbf{B}^{eT} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{eT} \left\{ \int_{S^e} \mathbf{N}^{eT} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{eT} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{eT} \bar{\mathbf{K}}^e \mathbf{T}^e \mathbf{d} = \sum_{e=1}^E \mathbf{T}^{eT} \bar{\mathbf{p}}_b^e + \sum_{e=1}^E \mathbf{T}^{eT} \bar{\mathbf{p}}^e$$

\mathbf{K} \mathbf{p}_b \mathbf{p}

Equilibrium equation of discretized structure

Equilibrium equation

$$\sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{V^e} \mathbf{B}^{e\text{T}} \boldsymbol{\sigma}^e dV^e \right\} = \sum_{e=1}^E \mathbf{T}^{e\text{T}} \left\{ \int_{S^e} \mathbf{N}^{e\text{T}} \mathbf{t}^e dS^e + \int_{V^e} \mathbf{N}^{e\text{T}} \mathbf{f}^e dV^e \right\}$$

Consideration of kinematic and constitutive equations

linear elasticity: $\boldsymbol{\sigma} = \mathbf{D}\boldsymbol{\varepsilon}$

linear kinematic relation: $\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}$

$$\boldsymbol{\sigma}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{u}^e = \mathbf{D}^e \mathbf{L}^e \mathbf{N}^e \mathbf{d}^e = \mathbf{D}^e \mathbf{B}^e \mathbf{T}^e \mathbf{d}$$

Equilibrium equation

$$\mathbf{K}\mathbf{d} = \mathbf{p}_b + \mathbf{p}$$

Plane stress ($\sigma_z = 0$)

Displacement vector

$$\mathbf{u} = \{u(x, y), v(x, y)\}$$

Strain vector

$$\boldsymbol{\varepsilon} = \{\varepsilon_x, \varepsilon_y, \gamma_{xy}\}$$

Stress vector

$$\boldsymbol{\sigma} = \{\sigma_x, \sigma_y, \tau_{xy}\}$$

Traction vector

$$\mathbf{t} = \{t_x, t_y\}$$

Body force intensity vector

$$\mathbf{f} = \{f_x, f_y\}$$

Constitutive matrix

$$\mathbf{D} = \frac{E}{1 - \nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix}$$

Differential operator matrix

$$\mathbf{L} = \begin{bmatrix} \frac{\partial}{\partial x} & 0 \\ 0 & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} \end{bmatrix}$$

Plane stress ($\sigma_z = 0$)

Stiffness matrix

$$\mathbf{k}^e = \int_{A^e} \mathbf{B}^{eT} \mathbf{D}^e \mathbf{B}^e h^e dA^e$$

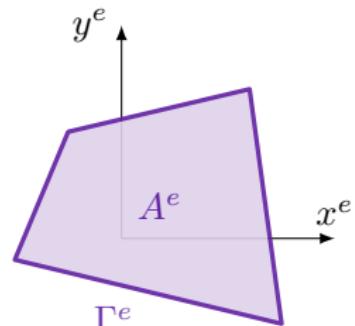
A^e, h^e – FE area and thickness, resp.

Element loading vector

$$\mathbf{p}^e = \int_{A^e} \mathbf{N}^{eT} \mathbf{f}^e h^e dA^e$$

Boundary loading vector

$$\mathbf{p}_b^e = \int_{\Gamma^e} \mathbf{N}^{eT} \mathbf{t}^e h^e d\Gamma^e$$

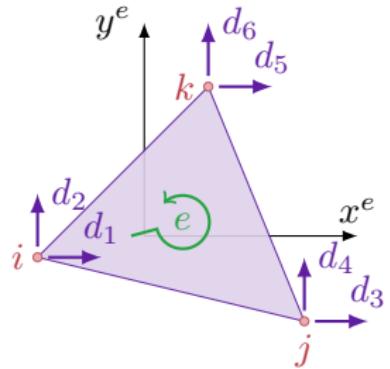


FEs for panels

Three-noded element

$$\mathbf{u}^e(x, y) = \mathbf{N}^e(x, y) \mathbf{d}^e$$

$$\mathbf{N}^e = \begin{bmatrix} N_i^e & 0 & N_j^e & 0 & N_k^e & 0 \\ 0 & N_i^e & 0 & N_j^e & 0 & N_k^e \end{bmatrix}, \quad \mathbf{d}^e = \begin{bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{bmatrix}$$

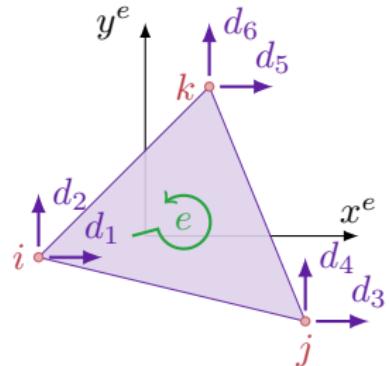


FEs for panels

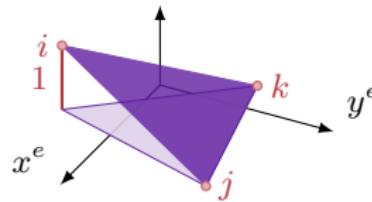
Three-noded element

$$\mathbf{u}^e(x, y) = \mathbf{N}^e(x, y) \mathbf{d}^e$$

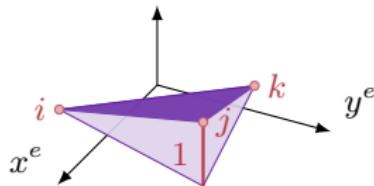
$$\mathbf{N}^e = \begin{bmatrix} N_i^e & 0 & N_j^e & 0 & N_k^e & 0 \\ 0 & N_i^e & 0 & N_j^e & 0 & N_k^e \end{bmatrix}, \quad \mathbf{d}^e = \begin{bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{bmatrix}$$



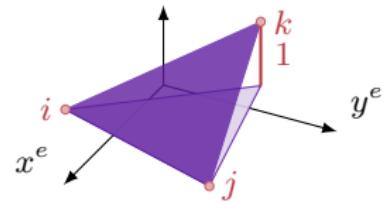
$$N_i(x^e, y^e)$$



$$N_j(x^e, y^e)$$



$$N_k(x^e, y^e)$$



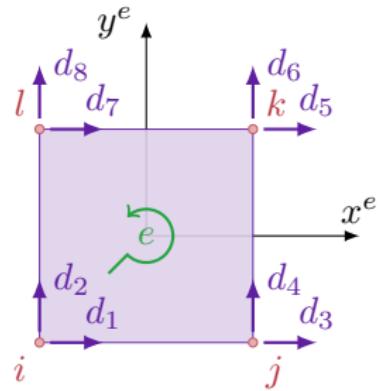
FEs for panels

Four-noded element

$$\mathbf{u}^e(x, y) = \mathbf{N}^e(x, y) \mathbf{d}^e$$

$$\mathbf{N}^e = \begin{bmatrix} N_i^e & 0 & N_j^e & 0 & N_k^e & 0 & N_l^e & 0 \\ 0 & N_i^e & 0 & N_j^e & 0 & N_k^e & 0 & N_l^e \end{bmatrix}$$

$$\mathbf{d}^e = \{d_1, d_2, d_3, d_4, d_5, d_6, d_7, d_8\}$$



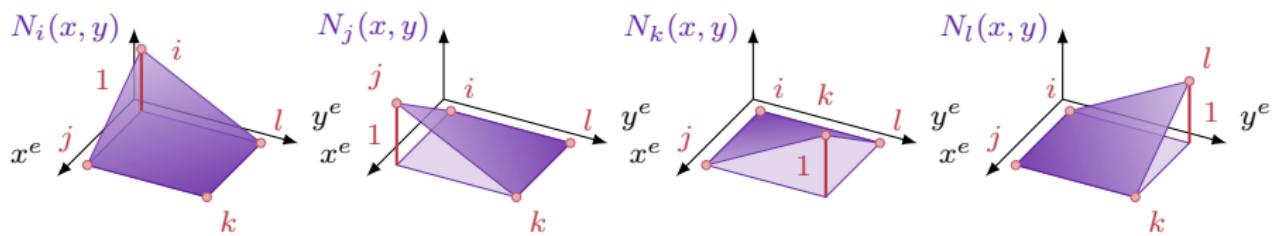
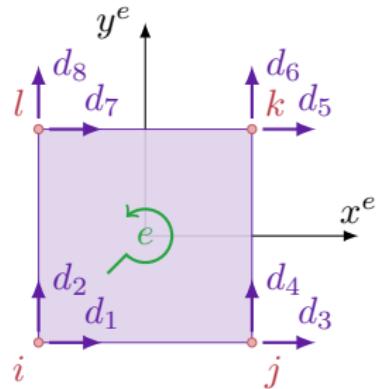
FEs for panels

Four-noded element

$$\mathbf{u}^e(x, y) = \mathbf{N}^e(x, y) \mathbf{d}^e$$

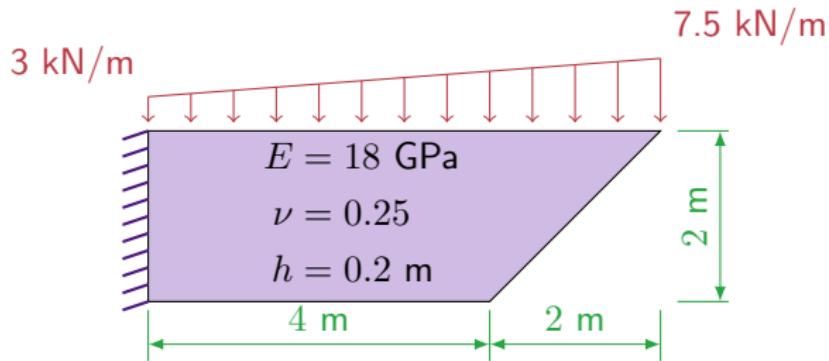
$$\mathbf{N}^e = \begin{bmatrix} N_i^e & 0 & N_j^e & 0 & N_k^e & 0 & N_l^e & 0 \\ 0 & N_i^e & 0 & N_j^e & 0 & N_k^e & 0 & N_l^e \end{bmatrix}$$

$$\mathbf{d}^e = \{d_1, d_2, d_3, d_4, d_5, d_6, d_7, d_8\}$$



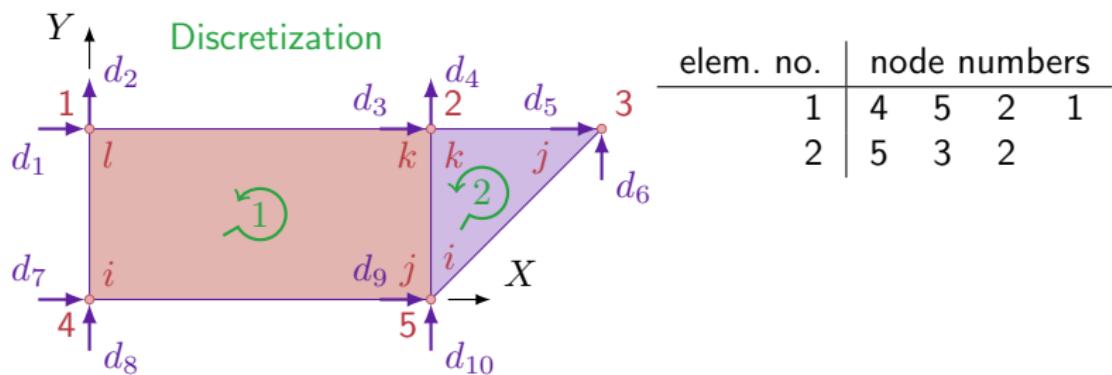
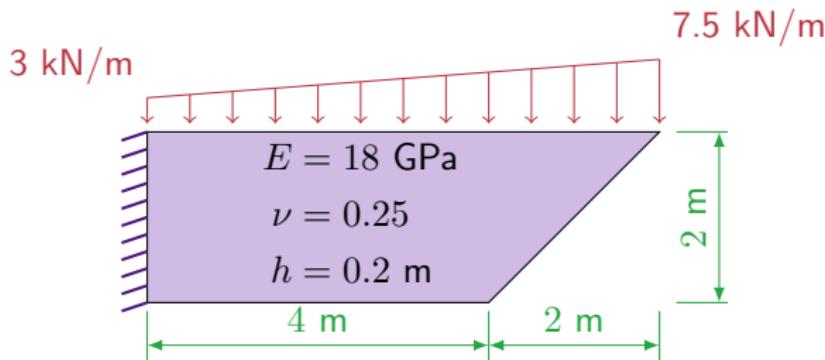
Example

Statics of a panel



Example

Statics of a panel

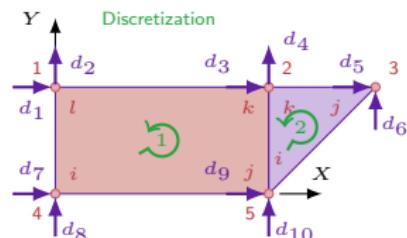
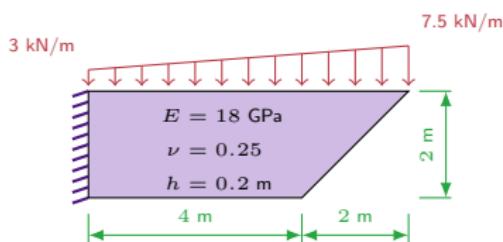


Example

Statics of a panel

Constitutive matrix

$$\mathbf{D} = \frac{18 \cdot 10^6}{1 - 0.25^2} \begin{bmatrix} 1 & 0.25 & 0 \\ 0.25 & 1 & 0 \\ 0 & 0 & \frac{1-0.25}{2} \end{bmatrix} [\text{kPa}]$$



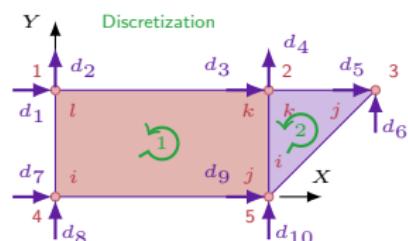
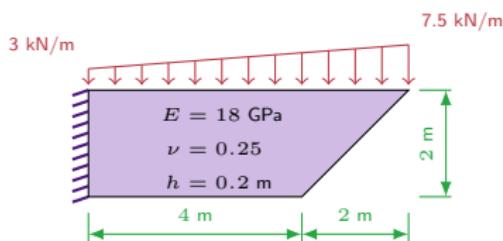
Example

Statics of a panel

Constitutive matrix

$$\mathbf{D} = \frac{18 \cdot 10^6}{1 - 0.25^2} \begin{bmatrix} 1 & 0.25 & 0 \\ 0.25 & 1 & 0 \\ 0 & 0 & \frac{1-0.25}{2} \end{bmatrix} [\text{kPa}]$$

$$\mathbf{D} = \begin{bmatrix} 19.2 & 4.8 & 0 \\ 4.8 & 19.2 & 0 \\ 0 & 0 & 7.2 \end{bmatrix} \cdot 10^6 [\text{kPa}]$$



Example

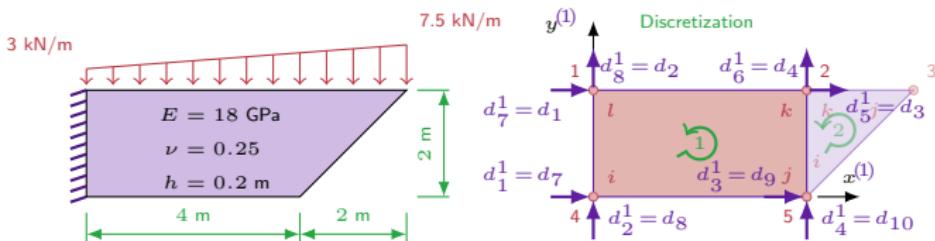
Statics of a panel

Shape functions – Element 1

$$N_i^1(x^{(1)}, y^{(1)}) = \frac{x^{(1)}y^{(1)} - 2x^{(1)} - 4y^{(1)} + 8}{8}, \quad N_k^1(x^{(1)}, y^{(1)}) = \frac{x^{(1)}y^{(1)}}{8}$$

$$N_j^1(x^{(1)}, y^{(1)}) = -\frac{x^{(1)}y^{(1)} - 2x^{(1)}}{8}, \quad N_l^1(x^{(1)}, y^{(1)}) = -\frac{x^{(1)}y^{(1)} - 4y^{(1)}}{8}$$

$$\mathbf{N}^1 = \begin{bmatrix} N_i^1 & 0 & N_j^1 & 0 & N_k^1 & 0 & N_l^1 & 0 \\ 0 & N_i^1 & 0 & N_j^1 & 0 & N_k^1 & 0 & N_l^1 \end{bmatrix}$$

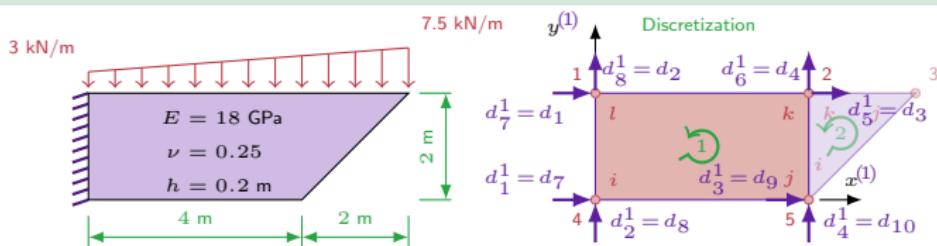


Example

Statics of a panel

Matrix \mathbf{K} – Element 1

$$\mathbf{B}^1(x^{(1)}, y^{(1)}) = \begin{bmatrix} \frac{y^{(1)}}{8} - \frac{1}{4} & 0 & \frac{1}{4} - \frac{y^{(1)}}{8} & 0 & \frac{y^{(1)}}{8} & 0 & -\frac{y^{(1)}}{8} & 0 \\ 0 & \frac{x^{(1)}}{8} - \frac{1}{2} & 0 & -\frac{x^{(1)}}{8} & 0 & \frac{x^{(1)}}{8} & 0 & \frac{1}{2} - \frac{x^{(1)}}{8} \\ \frac{x^{(1)}}{8} - \frac{1}{2} & \frac{y^{(1)}}{8} - \frac{1}{4} & -\frac{x^{(1)}}{8} & \frac{1}{4} - \frac{y^{(1)}}{8} & \frac{x^{(1)}}{8} & \frac{y^{(1)}}{8} & \frac{1}{2} - \frac{x^{(1)}}{8} & -\frac{y^{(1)}}{8} \end{bmatrix}$$



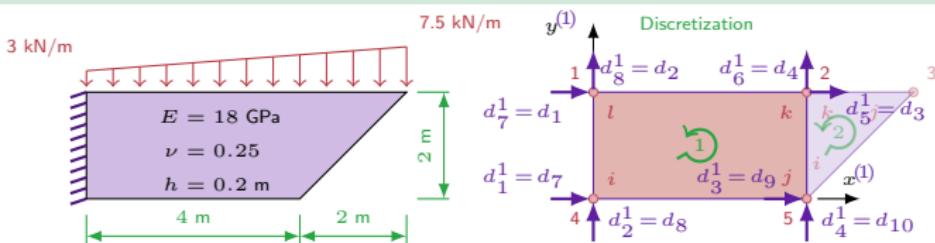
Example

Statics of a panel

Matrix \mathbf{K} – Element 1

$$\mathbf{B}^1(x^{(1)}, y^{(1)}) = \begin{bmatrix} \frac{y^{(1)}}{8} - \frac{1}{4} & 0 & \frac{1}{4} - \frac{y^{(1)}}{8} & 0 & \frac{y^{(1)}}{8} & 0 & -\frac{y^{(1)}}{8} & 0 \\ 0 & \frac{x^{(1)}}{8} - \frac{1}{2} & 0 & -\frac{x^{(1)}}{8} & 0 & \frac{x^{(1)}}{8} & 0 & \frac{1}{2} - \frac{x^{(1)}}{8} \\ \frac{x^{(1)}}{8} - \frac{1}{2} & \frac{y^{(1)}}{8} - \frac{1}{4} & -\frac{x^{(1)}}{8} & \frac{1}{4} - \frac{y^{(1)}}{8} & \frac{x^{(1)}}{8} & \frac{y^{(1)}}{8} & \frac{1}{2} - \frac{x^{(1)}}{8} & -\frac{y^{(1)}}{8} \end{bmatrix}$$

$$\mathbf{K}^1 = \int_0^2 \int_0^4 \mathbf{B}^{1T} \mathbf{D} \mathbf{B}^1 h \, dx^{(1)} dy^{(1)} = \begin{bmatrix} 16 & 6 & -1.6 & -1.2 & -8 & -6 & -6.4 & 1.2 \\ 6 & 28 & 1.2 & 10.4 & -6 & -14 & -1.2 & -24.4 \\ -1.6 & 1.2 & 16 & -6 & -6.4 & -1.2 & -8 & 6 \\ -1.2 & 10.4 & -6 & 28 & 1.2 & -24.4 & 6 & -14 \\ -8 & -6 & -6.4 & 1.2 & 16 & 6 & -1.6 & -1.2 \\ -6 & -14 & -1.2 & -24.4 & 6 & 28 & 1.2 & 10.4 \\ -6.4 & -1.2 & -8 & 6 & -1.6 & 1.2 & 16 & -6 \\ 1.2 & -24.4 & 6 & -14 & -1.2 & 10.4 & -6 & 28 \end{bmatrix} \cdot 10^5$$



Example

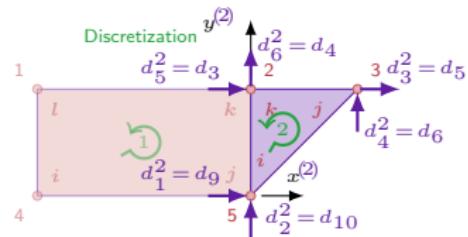
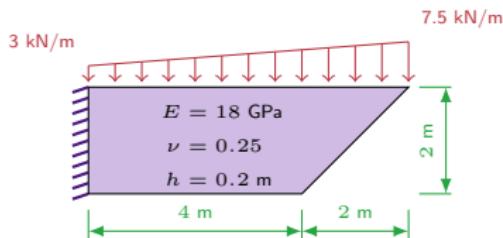
Statics of a panel

Shape functions – Element 2

$$N_i^2(x^{(2)}, y^{(2)}) = \frac{2 - y^{(2)}}{2}, \quad N_k^2(x^{(2)}, y^{(2)}) = \frac{y^{(2)} - x^{(2)}}{2}$$

$$N_j^2(x^{(2)}, y^{(2)}) = \frac{x^{(2)}}{2}$$

$$\mathbf{N}^2 = \begin{bmatrix} N_i^2 & 0 & N_j^2 & 0 & N_k^2 & 0 \\ 0 & N_i^2 & 0 & N_j^2 & 0 & N_k^2 \end{bmatrix}$$

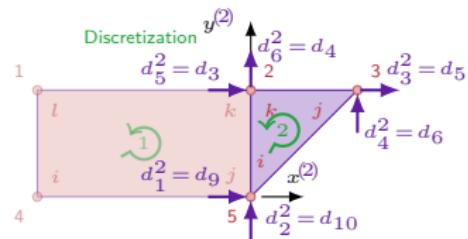
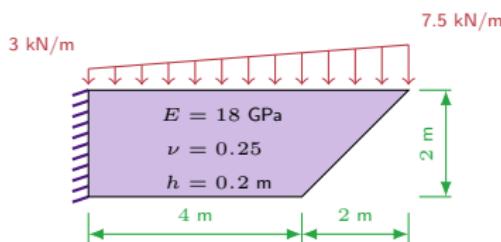


Example

Statics of a panel

Matrix \mathbf{K} – Element 2

$$\mathbf{B}^2(x^{(2)}, y^{(2)}) = \begin{bmatrix} 0 & 0 & \frac{1}{2} & 0 & -\frac{1}{2} & 0 \\ 0 & -\frac{1}{2} & 0 & 0 & 0 & \frac{1}{2} \\ -\frac{1}{2} & 0 & 0 & \frac{1}{2} & \frac{1}{2} & -\frac{1}{2} \end{bmatrix}$$



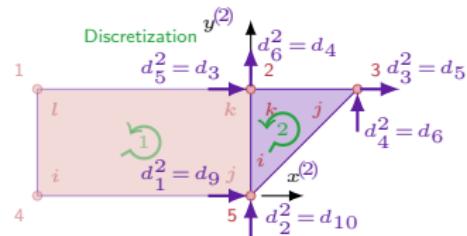
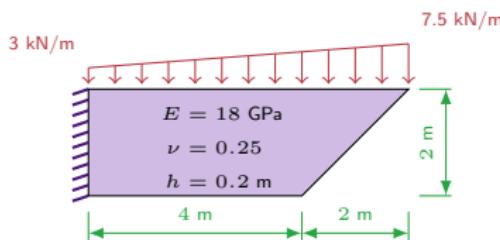
Example

Statics of a panel

Matrix \mathbf{K} – Element 2

$$\mathbf{B}^2(x^{(2)}, y^{(2)}) = \begin{bmatrix} 0 & 0 & \frac{1}{2} & 0 & -\frac{1}{2} & 0 \\ 0 & -\frac{1}{2} & 0 & 0 & 0 & \frac{1}{2} \\ -\frac{1}{2} & 0 & 0 & \frac{1}{2} & \frac{1}{2} & -\frac{1}{2} \end{bmatrix}$$

$$\mathbf{K}^2 = \mathbf{B}^{2T} \mathbf{D} \mathbf{B}^2 h A^2 = \begin{bmatrix} 7.2 & 0 & 0 & -7.2 & -7.2 & 7.2 \\ 0 & 19.2 & -4.8 & 0 & 4.8 & -19.2 \\ 0 & -4.8 & 19.2 & 0 & -19.2 & 4.8 \\ -7.2 & 0 & 0 & 7.2 & 7.2 & -7.2 \\ -7.2 & 4.8 & -19.2 & 7.2 & 26.4 & -12 \\ 7.2 & -19.2 & 4.8 & -7.2 & -12 & 26.4 \end{bmatrix} \cdot 10^5$$

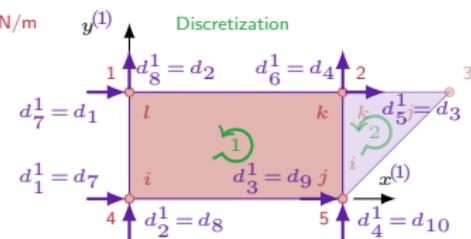
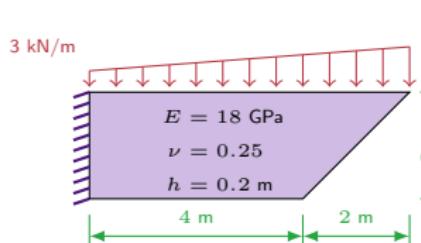


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\mathbf{P}_b^1 = \int_{\Gamma_{ij}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{jk}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{kl}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma$$



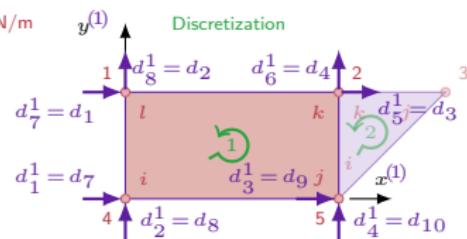
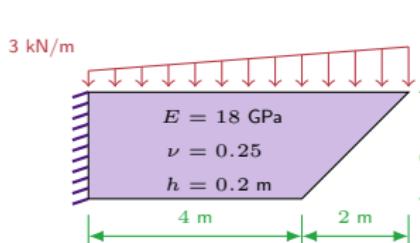
Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\mathbf{P}_b^1 = \int_{\Gamma_{ij}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{jk}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{kl}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma$$

b.c. = 0
interelem. edge
force balance
along line 2-5
 $\mathbf{t}_{jk}^1 = -\mathbf{t}_{ki}^2$

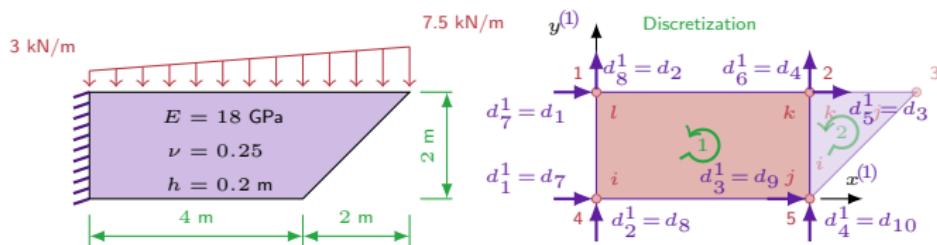


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\mathbf{P}_b^1 = \int_{\Gamma_{kl}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma$$

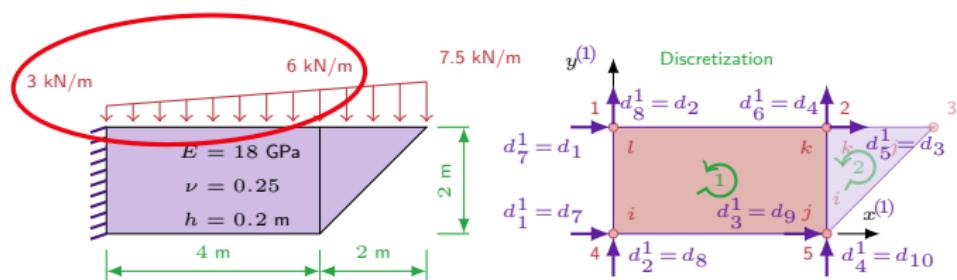


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\mathbf{P}_b^1 = \int_{\Gamma_{kl}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma + \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma$$
$$\int_{\Gamma_{kl}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma = \int_0^4 \left(\mathbf{N}^1(x^{(1)}, y^{(1)}=2) \right)^T \begin{bmatrix} 0 \\ -3 \left(1 - \frac{x^{(1)}}{4} \right) - 6 \frac{x^{(1)}}{4} \end{bmatrix} dx^{(1)}$$
$$= \{0 \ 0 \ 0 \ 0 \ 0 \ -10 \ 0 \ -8\}$$

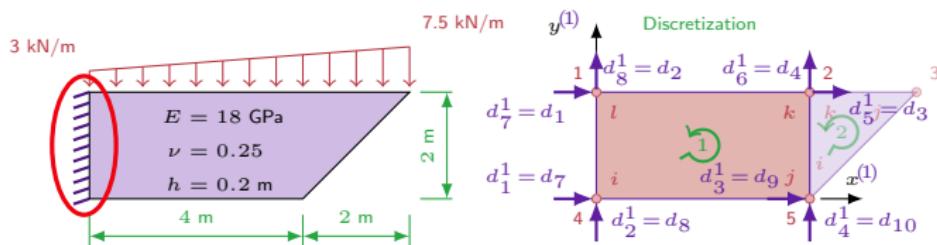


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\begin{aligned}\mathbf{P}_b^1 &= \{0\ 0\ 0\ 0\ 0\ -10\ 0\ -8\} + \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma \\ \int_{\Gamma_{li}^1} \mathbf{N}^{1T} \mathbf{t} d\Gamma &= \int_0^2 \left(\mathbf{N}^1(x^{(1)}=0, y^{(1)}) \right)^T \mathbf{t} dy^{(1)} \\ &= \{R_1^1\ R_2^1\ 0\ 0\ 0\ 0\ R_7^1\ R_8^1\}\end{aligned}$$



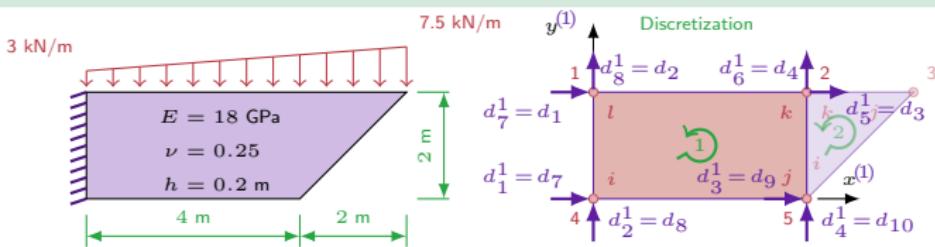
Example

Statics of a panel

Wektor \mathbf{P}_b – Element 1

$$\mathbf{P}_b^1 = \{0\ 0\ 0\ 0\ 0\ -10\ 0\ -8\} + \{R_1^1\ R_2^1\ 0\ 0\ 0\ 0\ R_7^1\ R_8^1\}$$

$$\mathbf{P}_b^1 = \begin{bmatrix} R_1^1 \\ R_2^1 \\ 0 \\ 0 \\ 0 \\ -10 \\ R_7^1 \\ R_8^1 - 8 \end{bmatrix}$$

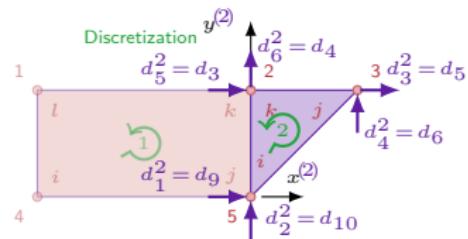
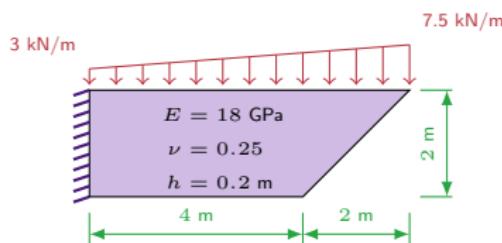


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 2

$$\mathbf{P}_b^2 = \int_{\Gamma_{ij}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma + \int_{\Gamma_{jk}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma + \int_{\Gamma_{ki}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma$$



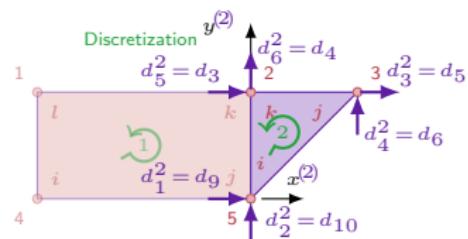
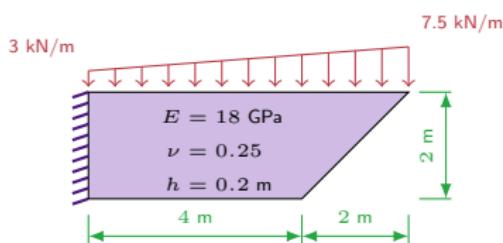
Example

Statics of a panel

Wektor \mathbf{P}_b – Element 2

$$\mathbf{P}_b^2 = \int_{\Gamma_{ij}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma + \int_{\Gamma_{jk}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma + \int_{\Gamma_{ki}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma$$

b.c. = 0
interelem. edge
force balance
along line 2-5
 $\mathbf{t}_{jk}^1 = -\mathbf{t}_{ki}^2$

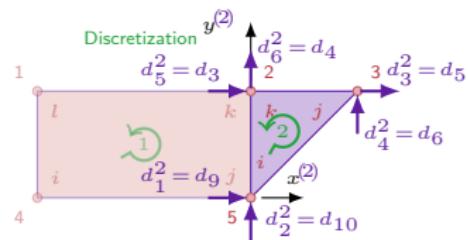
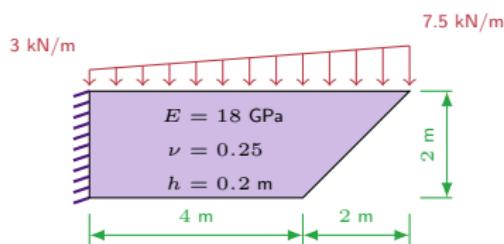


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 2

$$\mathbf{P}_b^2 = - \int_{\Gamma_{jk}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma$$



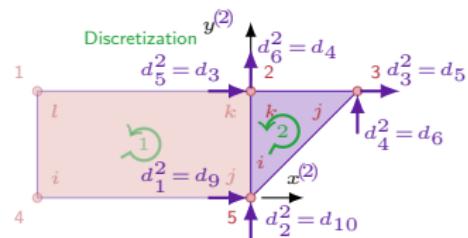
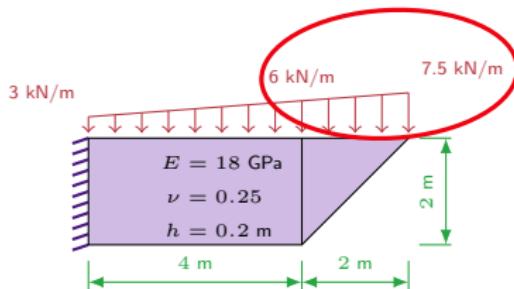
Example

Statics of a panel

Wektor \mathbf{P}_b – Element 2

$$\mathbf{P}_b^2 = - \int_{\Gamma_{jk}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma$$

$$\begin{aligned} \int_{\Gamma_{jk}^2} \mathbf{N}^{2T} \mathbf{t} d\Gamma &= \int_0^2 (\mathbf{N}^1(x^{(2)}, y^{(2)}=2))^T \left[\begin{array}{c} 0 \\ -6 \left(1 - \frac{x^{(2)}}{2}\right) - 7.5 \frac{x^{(2)}}{2} \end{array} \right] dx^{(2)} \\ &= \{0 \ 0 \ 0 \ -7 \ 0 \ -6.5\} \end{aligned}$$

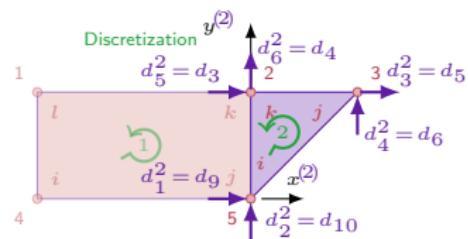
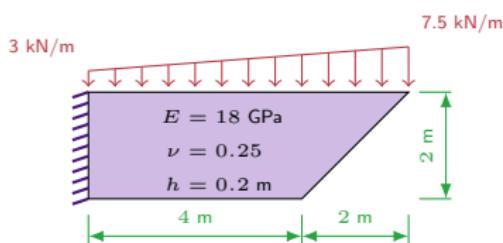


Example

Statics of a panel

Wektor \mathbf{P}_b – Element 2

$$\mathbf{P}_b^2 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ -7 \\ 0 \\ -6.5 \end{bmatrix}$$



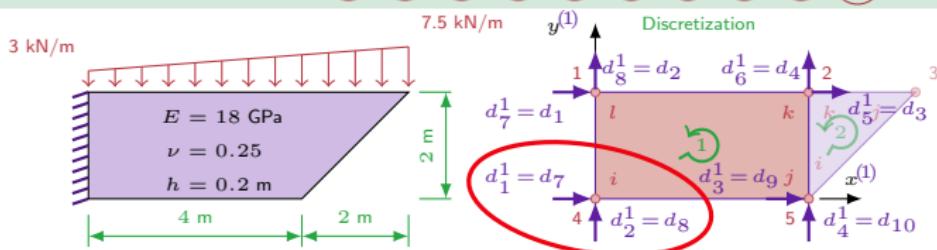
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^1 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ (1) \\ (2) \\ (3) \\ (4) \\ (5) \\ (6) \\ (7) \\ (8) \end{array}$$

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)



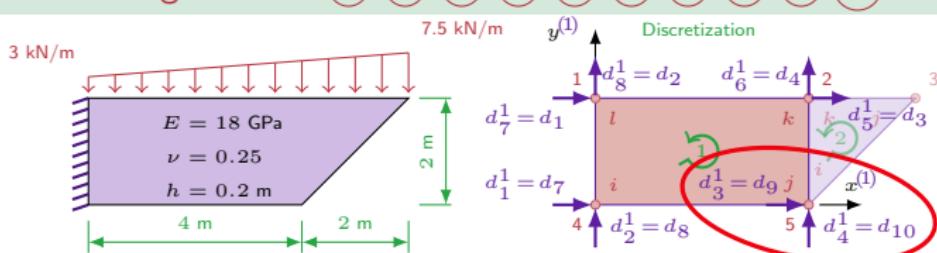
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^1 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ \textcircled{1} \\ \textcircled{2} \\ \textcircled{3} \\ \textcircled{4} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{7} \\ \textcircled{8} \end{array}$$

glob. no. \textcircled{1} \textcircled{2} \textcircled{3} \textcircled{4} \textcircled{5} \textcircled{6} \textcircled{7} \textcircled{8} \textcircled{9} \textcircled{10}



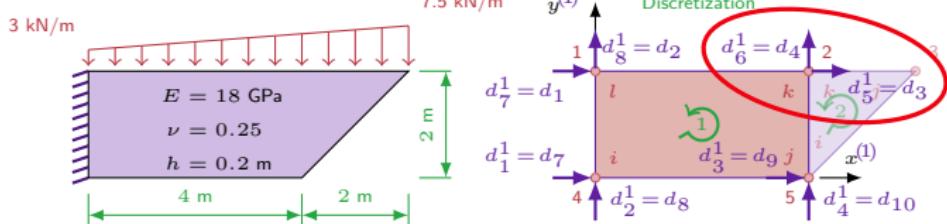
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^1 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ \textcircled{1} \\ \textcircled{2} \\ \textcircled{3} \\ \textcircled{4} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{7} \\ \textcircled{8} \end{array}$$

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)



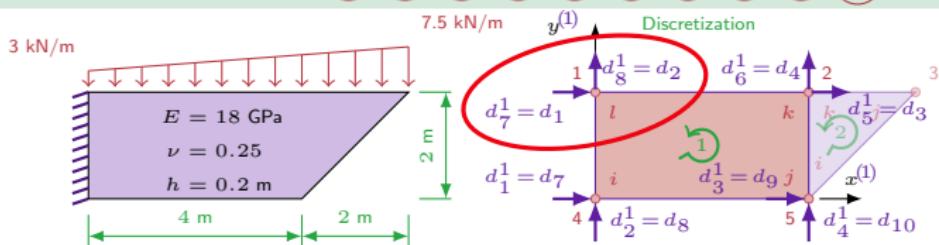
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^1 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ \textcircled{1} \\ \textcircled{2} \\ \textcircled{3} \\ \textcircled{4} \\ \textcircled{5} \\ \textcircled{6} \\ \textcircled{7} \\ \textcircled{8} \end{array}$$

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)



Example

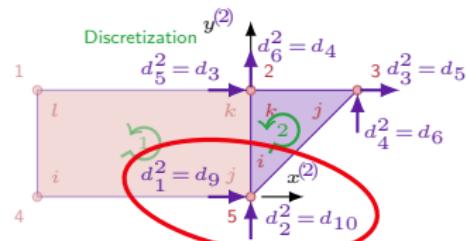
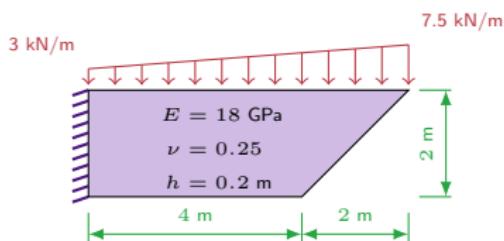
Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

loc. no.

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)



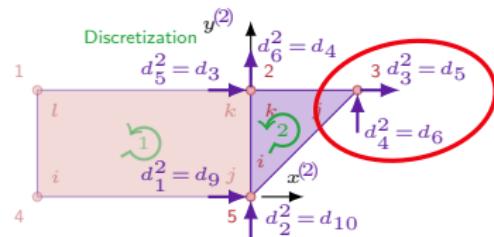
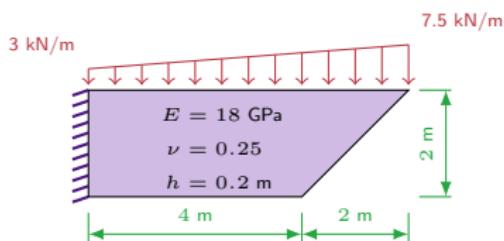
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ (1) \\ (2) \\ (3) \\ (4) \\ (5) \\ (6) \end{array}$$

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)



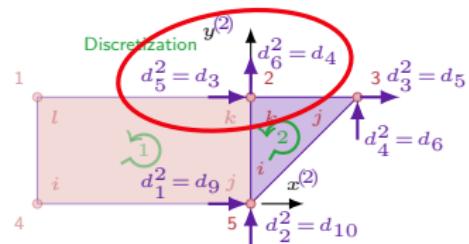
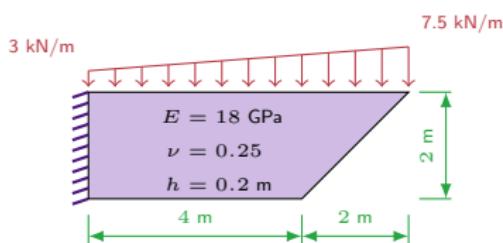
Example

Statics of a panel

Assembly – Boole's matrix \mathbf{B}

$$\mathbf{B}^2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{c} \text{loc. no.} \\ (1) \\ (2) \\ (3) \\ (4) \\ (5) \\ (6) \end{array}$$

glob. no. (1) (2) (3) (4) (5) (6) (7) (8) (9) (10)

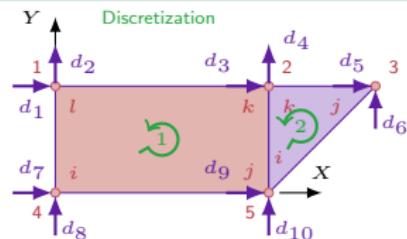
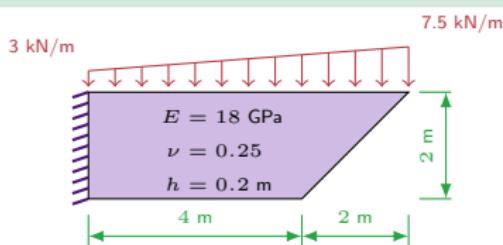


Example

Statics of a panel

Assembly - stiffness matrix

$$\mathbf{K} = \mathbf{B}^1{}^T \mathbf{K}^1 \mathbf{B}^1 + \mathbf{B}^2{}^T \mathbf{K}^2 \mathbf{B}^2$$



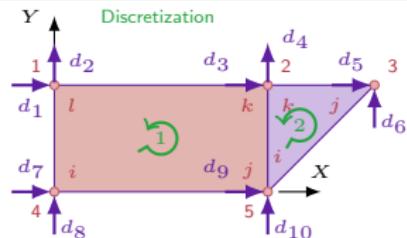
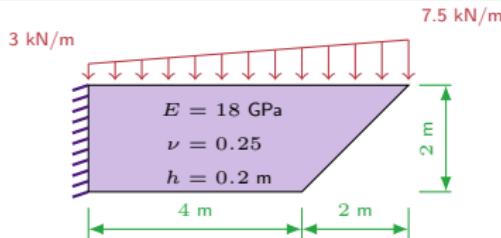
Example

Statics of a panel

Assembly - stiffness matrix

$$\mathbf{K} = \mathbf{B}^1{}^T \mathbf{K}^1 \mathbf{B}^1 + \mathbf{B}^2{}^T \mathbf{K}^2 \mathbf{B}^2$$

$$\mathbf{K} = \begin{bmatrix} 16 & -6 & -1.6 & 1.2 & 0 & 0 & -6.4 & -1.2 & -8 & 6 \\ -6 & 28 & -1.2 & 10.4 & 0 & 0 & 1.2 & -24.4 & 6 & -14 \\ -1.6 & -1.2 & 42.4 & -6 & -19.2 & 7.2 & -8 & -6 & -13.6 & 6 \\ 1.2 & 10.4 & -6 & 54.4 & 4.8 & -7.2 & -6 & -14 & 6 & -43.6 \\ 0 & 0 & -19.2 & 4.8 & 19.2 & 0 & 0 & 0 & 0 & -4.8 \\ 0 & 0 & 7.2 & -7.2 & 0 & 7.2 & 0 & 0 & -7.2 & 0 \\ -6.4 & 1.2 & -8 & -6 & 0 & 0 & 16 & 6 & -1.6 & -1.2 \\ -1.2 & -24.4 & -6 & -14 & 0 & 0 & 6 & 28 & 1.2 & 10.4 \\ -8 & 6 & -13.6 & 6 & 0 & -7.2 & -1.6 & 1.2 & 23.2 & -6 \\ 6 & -14 & 6 & -43.6 & -4.8 & 0 & -1.2 & 10.4 & -6 & 47.2 \end{bmatrix} \cdot 10^5$$

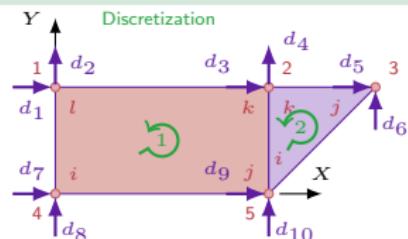
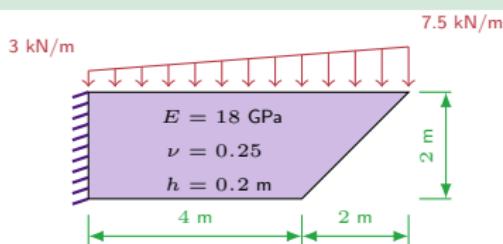


Example

Statics of a panel

Assembly - loading vector

$$\mathbf{P}_b = \mathbb{B}^{1^T} \mathbf{P}_b^1 + \mathbb{B}^{2^T} \mathbf{P}_b^2, \quad \mathbf{P} = \mathbf{0}$$



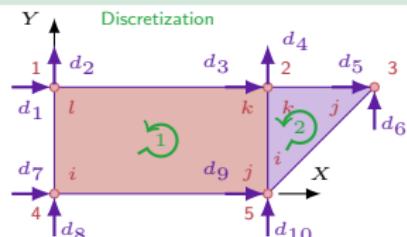
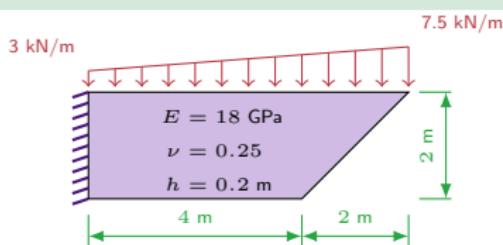
Example

Statics of a panel

Assembly - loading vector

$$\mathbf{P}_b = \mathbb{B}^{1^T} \mathbf{P}_b^1 + \mathbb{B}^{2^T} \mathbf{P}_b^2, \quad \mathbf{P} = \mathbf{0}$$

$$\mathbf{P}_b = \begin{bmatrix} 0 \\ -8 \\ 0 \\ -16.5 \\ 0 \\ -7 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} R_7^1 = R_1 \\ R_7^1 = R_2 \\ 0 \\ 0 \\ 0 \\ R_1^1 = R_7 \\ R_2^1 = R_8 \\ 0 \\ 0 \end{bmatrix}$$

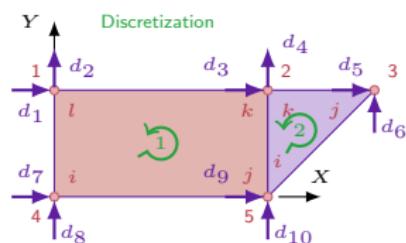
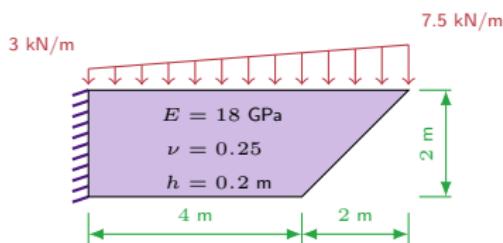


Example

Statics of a panel

FEM set of equations: $\mathbf{Kd} = \mathbf{P} + \mathbf{P}_b$

$$\left[\begin{array}{ccccccccc} 16 & -6 & -1.6 & 1.2 & 0 & 0 & -6.4 & -1.2 & -8 & 6 \\ -6 & 28 & -1.2 & 10.4 & 0 & 0 & 1.2 & -24.4 & 6 & -14 \\ -1.6 & -1.2 & 42.4 & -6 & -19.2 & 7.2 & -8 & -6 & -13.6 & 6 \\ 1.2 & 10.4 & -6 & 54.4 & 4.8 & -7.2 & -6 & -14 & 6 & -43.6 \\ 0 & 0 & -19.2 & 4.8 & 19.2 & 0 & 0 & 0 & 0 & -4.8 \\ 0 & 0 & 7.2 & -7.2 & 0 & 7.2 & 0 & 0 & -7.2 & 0 \\ -6.4 & 1.2 & -8 & -6 & 0 & 0 & 16 & 6 & -1.6 & -1.2 \\ -1.2 & -24.4 & -6 & -14 & 0 & 0 & 6 & 28 & 1.2 & 10.4 \\ -8 & 6 & -13.6 & 6 & 0 & -7.2 & -1.6 & 1.2 & 23.2 & -6 \\ 6 & -14 & 6 & -43.6 & -4.8 & 0 & -1.2 & 10.4 & -6 & 47.2 \end{array} \right] \cdot 10^5 = \left[\begin{array}{c} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \\ d_7 \\ d_8 \\ d_9 \\ d_{10} \end{array} \right] = \left[\begin{array}{c} 0 \\ -8 \\ 0 \\ 0 \\ -16.5 \\ 0 \\ -7 \\ 0 \\ 0 \\ 0 \end{array} \right] + \left[\begin{array}{c} R_1 \\ R_2 \\ R_3 \\ R_4 \\ R_5 \\ R_6 \\ R_7 \\ R_8 \\ R_9 \\ R_{10} \end{array} \right]$$

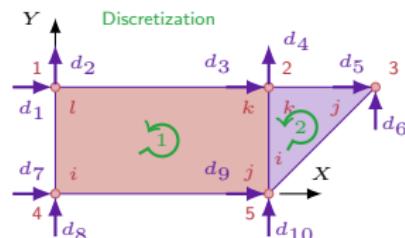
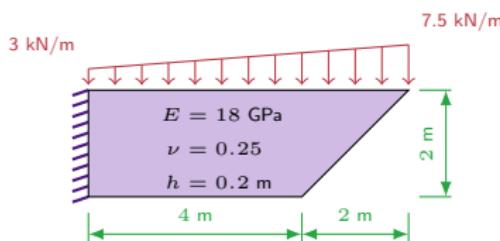


Example

Statics of a panel

FEM set of equations: $\mathbf{Kd} = \mathbf{P} + \mathbf{P}_b$

$$\begin{bmatrix} 16 & -6 & -1.6 & 1.2 & 0 & 0 & -6.4 & -1.2 & -8 & 6 \\ -6 & 28 & -1.2 & 10.4 & 0 & 0 & 1.2 & -24.4 & 6 & -14 \\ -1.6 & -1.2 & 42.4 & -6 & -19.2 & 7.2 & -8 & -6 & -13.6 & 6 \\ 1.2 & 10.4 & -6 & 54.4 & 4.8 & -7.2 & -6 & -14 & 6 & -43.6 \\ 0 & 0 & -19.2 & 4.8 & 19.2 & 0 & 0 & 0 & 0 & -4.8 \\ 0 & 0 & 7.2 & -7.2 & 0 & 7.2 & 0 & 0 & -7.2 & 0 \\ -6.4 & 1.2 & -8 & -6 & 0 & 0 & 16 & 6 & -1.6 & -1.2 \\ -1.2 & -24.4 & -6 & -14 & 0 & 0 & 6 & 28 & 1.2 & 10.4 \\ -8 & 6 & -13.6 & 6 & 0 & -7.2 & -1.6 & 1.2 & 23.2 & -6 \\ 6 & -14 & 6 & -43.6 & -4.8 & 0 & -1.2 & 10.4 & -6 & 47.2 \end{bmatrix} \cdot 10^5 = \begin{bmatrix} 0 \\ 0 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \\ 0 \\ 0 \\ d_9 \\ d_{10} \end{bmatrix} = \begin{bmatrix} 0 \\ -8 \\ 0 \\ 0 \\ 0 \\ -7 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} R_1 \\ R_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ R_7 \\ R_8 \\ 0 \\ 0 \end{bmatrix}$$



Example

Statics of a panel

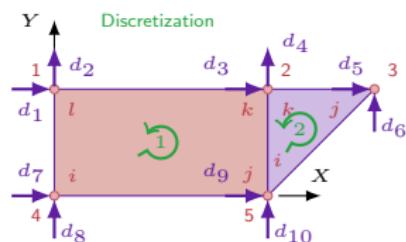
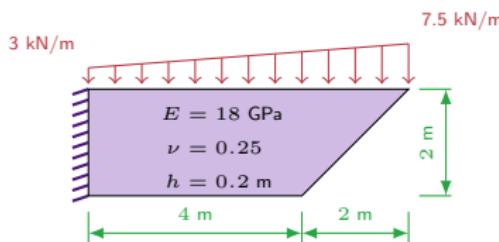
FEM set of equations: $\mathbf{Kd} = \mathbf{P} + \mathbf{P}_b$

$$\begin{bmatrix} 16 & -6 & -1.6 & 1.2 & 0 & 0 & -6.4 & -1.2 & -8 & 6 \\ -6 & 28 & -1.2 & 10.4 & 0 & 0 & 1.2 & -24.4 & 6 & -14 \\ -1.6 & -1.2 & 42.4 & -6 & -19.2 & 7.2 & -8 & -6 & -13.6 & 6 \\ 1.2 & 10.4 & -6 & 54.4 & 4.8 & -7.2 & -6 & -14 & 6 & -43.6 \\ 0 & 0 & -19.2 & 4.8 & 19.2 & 0 & 0 & 0 & 0 & -4.8 \\ 0 & 0 & 7.2 & -7.2 & 0 & 7.2 & 0 & 0 & -7.2 & 0 \\ -6.4 & 1.2 & -8 & -6 & 0 & 0 & 16 & 6 & -1.6 & -1.2 \\ -1.2 & -24.4 & -6 & -14 & 0 & 0 & 6 & 28 & 1.2 & 10.4 \\ -8 & 6 & -13.6 & 6 & 0 & -7.2 & -1.6 & 1.2 & 23.2 & -6 \\ 6 & -14 & 6 & -43.6 & -4.8 & 0 & -1.2 & 10.4 & -6 & 47.2 \end{bmatrix} \cdot 10^5 = \begin{bmatrix} 0 \\ 0 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \\ 0 \\ 0 \\ d_9 \\ d_{10} \end{bmatrix} = \begin{bmatrix} 0 \\ -8 \\ 0 \\ 0 \\ 0 \\ -7 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} R_1 \\ R_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ R_7 \\ R_8 \\ 0 \\ 0 \end{bmatrix}$$

Solution:

$$\mathbf{d} = \{0 \ 0 \ 3.881 \ -11.03 \ 3.949 \ -19.62 \ 0 \ 0 \ -3.744 \ -10.75\} \cdot 10^{-5} \text{ m}$$

$$\mathbf{R} = \{-54 \ 16.744 \ 0 \ 0 \ 0 \ 54 \ 14.756 \ 0 \ 0\} \text{ kN}$$

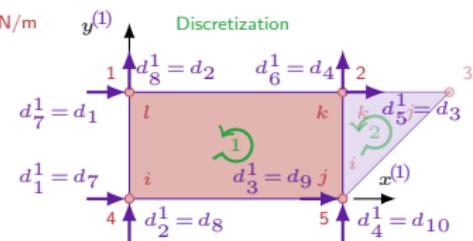
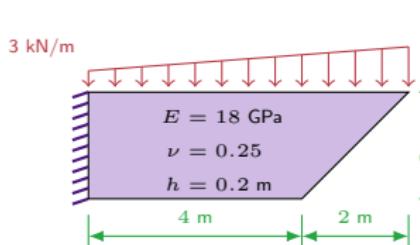


Example

Statics of a panel

Return to element: Element 1

$$\mathbf{d}^1 = \mathbf{B}^1 \mathbf{d} = \{0 \ 0 \ -3.744 \ -10.75 \ 3.881 \ -11.03 \ 0 \ 0\} \cdot 10^{-5}$$



Example

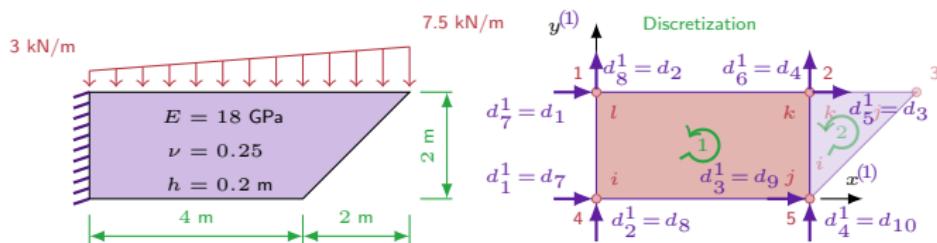
Statics of a panel

Return to element: Element 1

$$\mathbf{d}^1 = \mathbf{B}^1 \mathbf{d} = \{0 \ 0 \ -3.744 \ -10.75 \ 3.881 \ -11.03 \ 0 \ 0\} \cdot 10^{-5}$$

$$\boldsymbol{\varepsilon}^1 = \mathbf{B}^1 \mathbf{d}^1$$

$$\boldsymbol{\varepsilon}^1 = \begin{bmatrix} 0.953y - 0.936 \\ -0.034x \\ 0.953x - 0.034y - 2.688 \end{bmatrix} \cdot 10^{-5}, \quad \boldsymbol{\varepsilon}^1(2,1) = \begin{bmatrix} 1.708 \\ 6.831 \\ -81.600 \end{bmatrix} \cdot 10^{-7}$$



Example

Statics of a panel

Return to element: Element 1

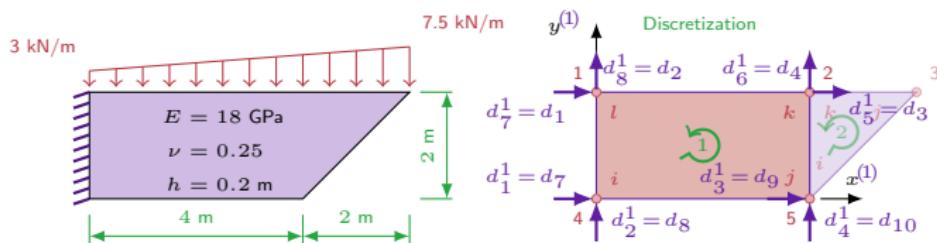
$$\mathbf{d}^1 = \mathbf{B}^1 \mathbf{d} = \{0 \ 0 \ -3.744 \ -10.75 \ 3.881 \ -11.03 \ 0 \ 0\} \cdot 10^{-5}$$

$$\boldsymbol{\varepsilon}^1 = \mathbf{B}^1 \mathbf{d}^1$$

$$\boldsymbol{\varepsilon}^1 = \begin{bmatrix} 0.953y - 0.936 \\ -0.034x \\ 0.953x - 0.034y - 2.688 \end{bmatrix} \cdot 10^{-5}, \quad \boldsymbol{\varepsilon}^1(2,1) = \begin{bmatrix} 1.708 \\ 6.831 \\ -81.600 \end{bmatrix} \cdot 10^{-7}$$

$$\boldsymbol{\sigma}^1 = \mathbf{D} \boldsymbol{\varepsilon}^1$$

$$\boldsymbol{\sigma}^1 = \begin{bmatrix} 182.976y - 179.712 - 1.632x \\ 45.744y - 44.928 - 6.528x \\ 68.616x - 2.448y - 193.536 \end{bmatrix}, \quad \boldsymbol{\sigma}^1(2,1) = \begin{bmatrix} 0 \\ -12.297 \\ -58.750 \end{bmatrix} \text{ kPa}$$

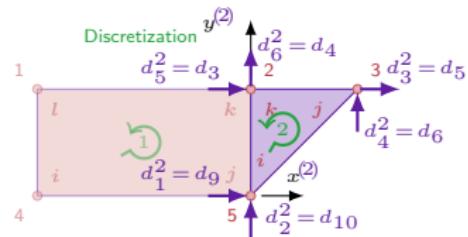
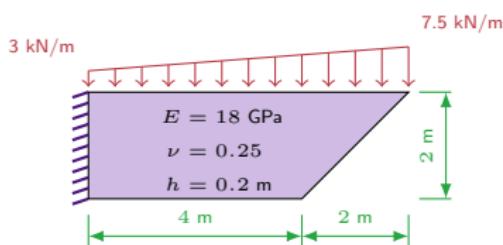


Example

Statics of a panel

Return to element: Element 2

$$\mathbf{d}^2 = \mathbf{B}^2 \mathbf{d} = \{-3.744 \ -10.75 \ 3.949 \ -19.62 \ 3.881 \ -11.03\} \cdot 10^{-5}$$



Example

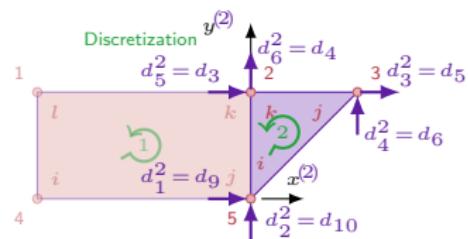
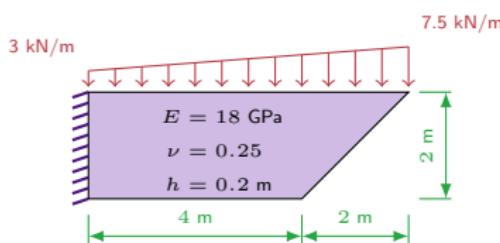
Statics of a panel

Return to element: Element 2

$$\mathbf{d}^2 = \mathbf{B}^2 \mathbf{d} = \{-3.744 \ -10.75 \ 3.949 \ -19.62 \ 3.881 \ -11.03\} \cdot 10^{-5}$$

$$\boldsymbol{\varepsilon}^2 = \mathbf{B}^2 \mathbf{d}^2$$

$$\boldsymbol{\varepsilon}^2 = \begin{bmatrix} 3.416 \\ 13.660 \\ -48.610 \end{bmatrix} \cdot 10^{-7}$$



Example

Statics of a panel

Return to element: Element 2

$$\mathbf{d}^2 = \mathbf{B}^2 \mathbf{d} = \{-3.744 \ -10.75 \ 3.949 \ -19.62 \ 3.881 \ -11.03\} \cdot 10^{-5}$$

$$\boldsymbol{\varepsilon}^2 = \mathbf{B}^2 \mathbf{d}^2$$

$$\boldsymbol{\varepsilon}^2 = \begin{bmatrix} 3.416 \\ 13.660 \\ -48.610 \end{bmatrix} \cdot 10^{-7}$$

$$\boldsymbol{\sigma}^2 = \mathbf{D} \boldsymbol{\varepsilon}^2$$

$$\boldsymbol{\sigma}^2 = \begin{bmatrix} 0 \\ -24.593 \\ -35.000 \end{bmatrix} \text{ kPa}$$

